

Isolation Enhancement using CSRR Slot in the Ground for Compact Two-Element Textile MIMO Antenna

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Abstract – A textile integrated, two-element, multiple-input multiple-output (MIMO) antenna is designed for Wi-Fi, wireless local area network (WLAN), and wearable biomedical applications. A CSRR slot and horn-shaped decoupling structure increases impedance matching and reduces the current movement from one element of antenna to another element which increases the isolation to 7.4 dB. The CSRR slot in the ground is accomplished between the elements to mitigate the surface current and enhance the isolation up to 27.4 dB. The 10-dB radiation exists from 4.65 to 5.97 GHz with more than 20-dB isolation in the full operating band where the maximum isolation is found to be 49.45 dB at 4.7 GHz. MIMO parameters are investigated in a two-element antenna, in which acceptable results are obtained. Bending analysis and phantom analysis are performed for wearable applications which demonstrate the acceptable results.

Index Terms – Defected ground structure (DGS), flexible antenna, isolation enhancement, MIMO antenna, textile antenna.

I. INTRODUCTION

There has been an extreme influence of body worn antennas for communication system recently. To satisfy the demands of communication in today's scenario, the antenna has to be robust, flexible, cost effective, compact, and reliable for wearable applications [1]. Flexible and textile antenna could be easily incorporated in the wearable and portable devices, but accomplishing the antenna in the compact space is a challenging task for a researcher. Among several technologies of antenna design, the use of multiple-input multiple-output (MIMO) antenna is a popular choice because in MIMO, same data is sent as multiple signals simultaneously through multiple

antennas. This results in high data rate, diversity performance, high channel bandwidth, link reliability, high channel capacity, multiple transmission and reception capability, as well as spatial multiplexing [2, 3]. When multiple antennas are incorporated in small space, the distance between antennas is minimized due to which the mutual coupling increases and affects the MIMO parameters. High isolation between antenna elements could primarily be achieved in MIMO antennas by positioning the radiators at high distance ($> \lambda/2$) from each other so that mutual coupling is neutralized. This results in a large sized antenna that is not suitable for wearable applications. Other methods to escape mutual coupling is to place the radiator either perpendicularly [3] or at orthogonal positions [4, 5]. Extended ground structure [6] or a conductive line between the radiators [7] also considerably reduces the size of antenna by bringing the radiators closer. To further reduce the size, which is compatible to the requirements of wearable devices, several decoupling structures such as meander lines, slots, stubs, as well as metamaterial structures such as EBG and SRR are utilized. Meander line structures are easy to implement on rigid FR-4 substrate [8] and provide good isolation, but antennas have to compromise with flexibility. Meander lines are also implemented on flexible jeans substrate to enhance isolation [2], but this approach increases design and fabrication complexities. Alternatively, T-shaped [9–12] and E-shaped [13] stubs, vertical and horizontal slotted ground [14], funnel-shaped defected ground structure [15], neutralized line between the radiators along with defected partial ground [16], decoupling stubs [17], and combination of vertical and horizontal ground for enhanced isolation [14] are very common, easy to implement, and simpler approach on jeans substrate. Researchers had also utilized dielectric resonators along with annular rings [18] to curb mutual coupling. In [19], four-element CPW-fed MIMO antenna is proposed for UWB applications with CSRR notch,

where distance between antenna and parasitic stub is used to improve the isolation. Researchers have also used metamaterial structures such as H-shaped EBG [20] for isolation enhancement. Orthogonal feed with stubs [4], defected ground structures, and square patch with chamfered feed [21] are some of the hybrid structures deliberately utilized for improved isolation and reducing size of antenna.

An antenna with flexible textile substrate has the following advantages over their fixed counterparts.

- The antenna can be designed conformal, enabling it to fit to the design of the device. Flexible textile antennas are also shock resistant, especially applicable on fast moving devices or wearables such as shoes or wrist watch.
- Fabric antennas are environment friendly when disposed and are immune to high temperature deformations that may exist in antennas with fixed substrates.

There are several types of textile materials that are used as a substrate to design flexible antennas [22] where jeans material, popularly known as denim material, is an obvious choice for research on wearable antennas because of its rugged and long lasting quality [23], low cost, and time saving fabrication techniques [1]. The fabric is highly researched and the textile characteristics are rigorously studied [24] and dielectric constant is determined [25].

The proposed textile antenna could be used in wearable applications with the following novelty and technical contributions.

1. The proposed antenna design is modest as compared to other structures [2, 9, 16] and is integrated on most popular, rugged, flexible, easily available, and inexpensive jeans textile material.
2. The suggested decoupling structure in this work enhances the port to port isolation significantly up to 49.45 dB which is expressively higher than the other related works [2, 4, 13, 15, 17].
3. The antenna is analyzed on different curvatures and maintains its band for wireless local area network (WLAN), Wi-Fi, and 5.8 GHz (ISM) with minimal effect on impedance matching as well as isolation.
4. To analyze the on-body radiation effect of antenna, specific absorption rate (SAR) is obtained using four layered phantom model. The obtained SAR is 0.2680 W/Kg which is lower than other reported work [2, 13, 16].

The antenna is designed with required Wi-Fi, WLAN, and ISM band applications and fulfilled the compact and flexible requirement for wearable applications. The demonstration of human body effect on the

antenna is discussed in the manuscript where antenna is designed with traditional equations, explained in eqn (1)–(3), and CSRR mitigates the current which is explained in Figure 1 (f). The low envelope correlation coefficient (ECC) and high isolation ensures that the antenna can be used for wireless communication applications.

II. MIMO ANTENNA DESIGN AND EVOLUTION STEPS

The optimized, compact two-element MIMO antenna is fabricated on lossy [24, 26] jeans material of 1 mm thickness (dielectric constant, $\epsilon_r = 1.7$) [2, 6, 24] which is illustrated in Figure 1 (a) with a prototype in hardware as shown in Figure 1 (b). The edge-to-edge dimensions of the antenna are 28 mm (W_b) \times 24 mm (W_h). Primarily, we have to design a single element antenna and calculate the length (λ_g) and the width of the feed with help of eqn (1)–(3) [27]. In MIMO antenna design, two elements are incorporated with the conventional edge-to-edge distance.

$$\text{For } \frac{W}{h} > 1,$$

where W = width of the patch, and h = height of the substrate where dielectric constant (ϵ_r) for jeans (denim) material is 1.7.

The effective dielectric constant is given by

$$\epsilon_{\text{reff}} = \frac{\epsilon_r + 1}{2} + \frac{\epsilon_r - 1}{2} \left(1 + 12 \frac{h}{W} \right)^{-\frac{1}{2}}, \quad (1)$$

$$\lambda_g = \frac{300}{f} \sqrt{\epsilon_{\text{eff}}}, \quad (2)$$

where f = resonant frequency.

The characteristic impedance Z_0 can be given by

$$Z_0 = \frac{120\pi}{\sqrt{\epsilon_{\text{reff}}} \left[\frac{w}{h} + 1.393 + 0.667 \ln \left(\frac{w}{h} + 1.444 \right) \right]}. \quad (3)$$

For MIMO antenna, the two elements are placed minimum at the distance of $\lambda/4$ for considerable isolation. However, this distance could be reduced by using isolation structures such as SRR and EBG. The calculated feed is $W_1 = W_2 = 2.7$ mm (width) and $W_3 = W_4 = 13.6$ mm (height) with $Z_0 = 52.36 \Omega$.

Other dimensions of two-element MIMO antenna in mm are: $W_5 = 3.9$, $W_6 = 23$, $W_7 = 8.5$, $W_8 = 8$, $W_9 = 8.9$, $r_1 = 6.7$, $r_2 = 6.6$, $W_{10} = 1.5$, and $W_{11} = 1.5$. The simulation of flexible and textile MIMO antenna is performed on Ansys HFSS-19 simulation software.

The two-element MIMO is evolved in four major iterations/steps, as is demonstrated in Figure 1 (c). In step-1, the ground height is 3.9 mm with 13.6-mm microstrip feed height where feed width of 2.7 mm is used to achieve approximately 50- Ω impedance matching. The $|S_{11}|$ in dB exists from 4.75 to 5.69 GHz, whereas the averaged isolation is at 10 dB with highest isolation of 13.66 dB as revealed in Figures 1 (d) and

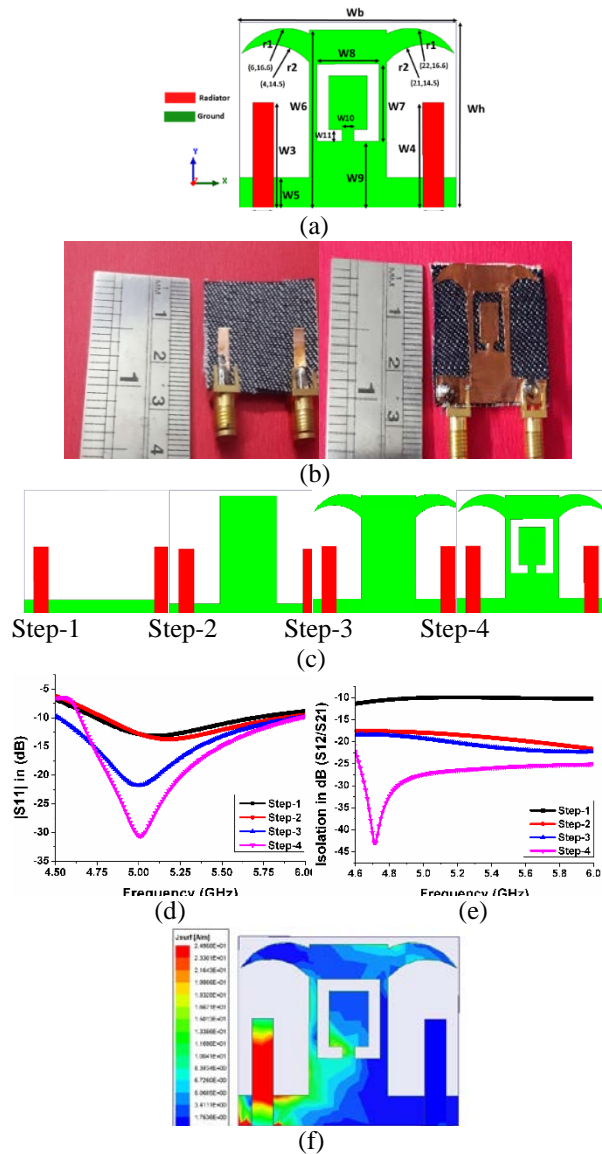


Fig. 1. (a) Proposed MIMO antenna (dimensions). (b) Prototype (fabricated). (c) Steps (evolution). (d) $|S_{11}|$ parameters (steps) in dB. (e) $|S_{12}|$ parameters (steps) in dB. (f) Surface current distribution at 5.8 GHz.

(e), respectively. In step-2, while increasing the ground vertically between two elements, isolation increases $|S_{21}|$ because this modification perturbs the current movement toward the modified ground structure from port one [6]. The $|S_{11}|$ in dB ranges from 4.80 to 5.87 GHz, whereas isolation is improved at this stage and ranges close to 17 dB, as is evident from Figures 1 (d) and (e). In step-3, a horn-shaped structure is implemented in the ground, which curates the impedance matching of antenna and increases the $|S_{11}|$ that varies from 4.53 to 5.96 GHz. The horn-shaped decoupling structure reduces the surface

current between antenna elements and improves the isolation by 7 dB. In the last step, CSRR slot is accomplished in the decoupling structure, thereby mitigating the surface current and improving the isolation up to 27 dB. The $|S_{11}|$ characteristics are further improved, which varies from 4.65 to 5.97 GHz with enhancement in isolation. The isolation at this stage has reached a peak of 49.45 dB, which is an improvement of 123.09% as compared to step-3 (without CSRR). Surface current analysis of two-port antenna is analyzed at 5.8 GHz which clearly demonstrates that the CSRR effectively diminishes the surface current and improves the isolation as shown in Figure 1 (f).

III. BENDING ANALYSIS OF ANTENNA

To study the performance of two-port antenna with structural deformations, the antenna is deliberately bent on a polystyrene base cylinder with diameter of 25, 20, 15, and 10 cm using the wrapping tool in HFSS 19 [28]. The cylinder is then removed and simulation is performed. The screenshots are shown in Figure 2 (a), whereas Figure 2 (b) depicts the placement of designed antenna on polystyrene base. The $|S_{11}|$ and $|S_{12}|$ characteristics in dB (simulated) are shown in Figures 2 (c) and (d). Figure 2 (f) shows the variation in radiation efficiency, where small variations are observed. The size of antenna is reducing and impedance matching varies when bending process is applied on two-port antenna; therefore, $|S_{11}|$ and $|S_{12}|$ are shifted toward higher frequency, where small variation is found [36]. The minimum variation is found in gain of antenna in bending process is due to small variations in efficiency as depicted in Figure 2 (e). The bending analysis proves that the proposed antenna is working effectively, without compromising with the radiating bandwidth and isolation.

IV. PHANTOM ANALYSIS

The wearable antennas are used near the human tissues; therefore, certain parameters of radiation have to be studied for wearable applications. The effect of radiation on different layers of human skin is measured in terms of SAR.

Absorption of electromagnetic (EM) energy when exposed to radiation of antenna is calculated in SAR. In other words, it is the radiated power absorbed by human tissue of 1 Kg, averaged at 1 or 10 g, as illustrated in eqn (4)

$$\text{SAR}_{\text{average}}(r, \omega) = \frac{1}{V} \int \frac{\sigma(r, \omega) |E(r, \omega)|^2}{2\rho(r)} dr, \quad (4)$$

where $|E(r, \omega)|$ is electrical field in volt/meter, V = volume in meter cube, r = position of vector, σ is sample density, and (r, ω) is the conductivity in Siemens/meter.

As per internationally approved standards, the value of SAR has to be under 1.6 W/Kg for safe use of antenna

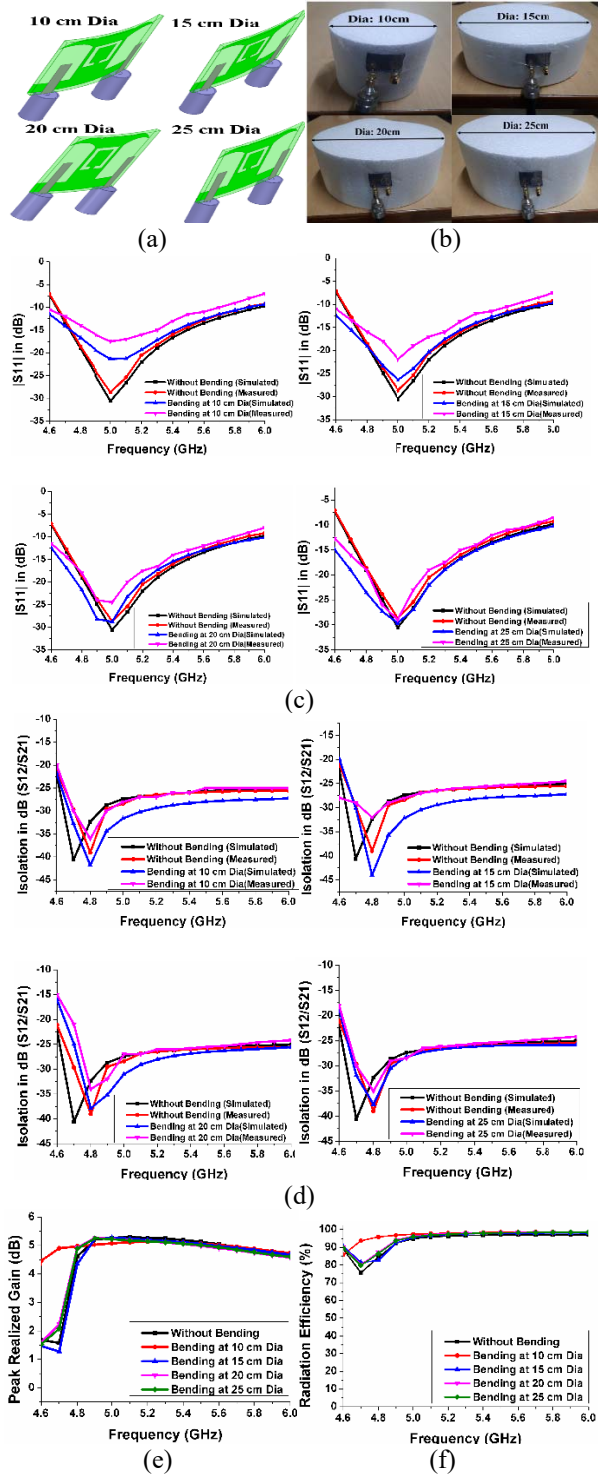


Fig. 2. Bending of antenna at 10, 15, 20, and 25 cm diameter (simulated). (b) Bending of antenna at 10, 15, 20, and 25 mm diameter (measured). (c) $|S_{11}|$ in dB for bending analysis (simulated and measured). (d) $|S_{12}/21|$ in dB for bending analysis (simulated and measured). (e) Peak realized gain variations on bending. (f) Radiation efficiency variations on bending.

Table 1: Characteristic values of human body tissues (5.8 GHz) [31]

Tissue	Conductivity (S/m)	Relative permittivity (ϵ_r)	Loss tangent (σ)
Skin	3.717	35.114	0.32807
Muscles	4.9616	48.485	0.31715
Fat	0.29313	4.9549	0.18335
Breast fat	0.41974	4.4976	0.28924
Bone	1.1544	9.6744	0.36981

near human body [29]. An analysis of the antenna positioned at 20-mm distance from a phantom model is performed. The phantom model (four layered) is composed of skin layer (2-mm thick), fat layer (3.5-mm thick), muscular layer (10-mm thick), and bone (10-mm thick) as depicted in Figure 3 (a). The tissue characteristics such as conductivity, loss tangent, and relative permittivity at 5.8-GHz frequency are given in Table 1. The $|S_{11}|$ and $|S_{12}|$ parameters of antenna in dB without phantom and with phantom are shown in Figures 3 (c) and (d). The minimum variations are observed in s-parameters when the four-layered phantom model is positioned at 20 mm from antenna, and this could be a feasible distance for wearable applications. The maximum SAR value was evaluated as 0.2680 W/Kg when averaged on 10 g of phantom model, when excited with a source power of 10 mW as is relevant from Figure 3 (b). The radiation efficiency and realized gain, in the absence and presence of phantom model, are depicted in Figures 3 (e) and (f), and a small variation in gain is found as a result of grating lobe reflection from the phantom model.

V. RESULTS AND DISCUSSIONS

The measurements were executed using VNA (Anritsu MS 2025B). The simulated and measured results of $|S_{11}|$ and $|S_{12}|$ in dB are depicted in Figures 4 (a) and (b), where $|S_{11}|$ in dB extends from 4.7 to 5.9 GHz with more than 20-dB isolation and minimum variation is found in the measured results. The anechoic chamber measurement for gain, where the amplitude of the transmitted signal (P_t) from MIMO is measured on the received signal (P_r) by horn antenna at a distance of 3 m. The gain is determined using formulae as given in eqn (5).

$$\frac{P_r}{P_t} = G_t G_r \left(\frac{\lambda}{4\pi d} \right)^2, \quad (5)$$

where G_t and G_r are antenna gains of the MIMO antenna and horn antenna, respectively, and d is the distance between the two antennas and λ is the measured wavelength. The realized gain varies

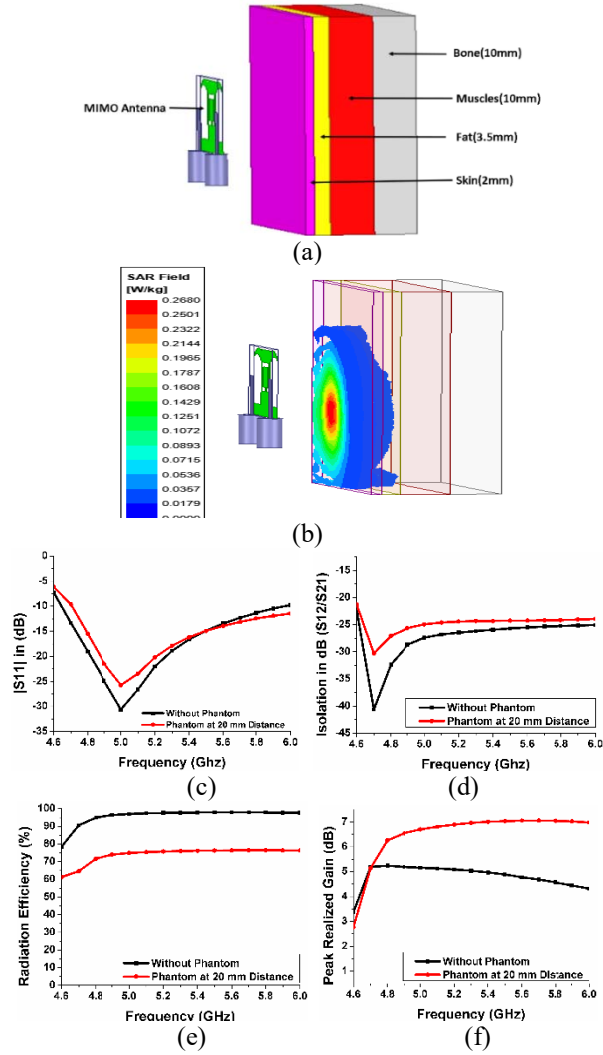


Fig. 3. Antenna positioned on phantom [30]. (b) Analysis of SAR (phantom). (c) $|S_{11}|$ in dB on phantom. (d) $|S_{12}|$ on phantom. (e) Radiation efficiency on phantom. (f) Peak realized gain on phantom.

from 3.37 to 5.23dB and less than 0.5 dB variation is observed with measured results due to environment losses associated with high frequency as depicted in Figure 4 (b). Radiation efficiency (simulated) is higher than 90% as is given in Figure 4 (c). The two-port antenna is measured on different body positions such as wrist, thigh, chest, and biceps for “on-body” wearable analysis as depicted in Figure 4 (f). The measured $|S_{11}|$ and $|S_{12}|$ in dB are depicted in Figures 4 (h) and (i). The results show that the antenna is performing satisfactorily when placed on any body part and also the antenna is able to maintain its isolation at less than 20 dB. Further, the antenna is placed on cap, shoes, bag, and riding helmet for portable wearable analysis as depicted in

Figure 4 (g), where the antenna has minimum variations in s -parameters due to coupling effect, but the experimental results show acceptable performance in terms of $|S_{11}|$ and $|S_{12}|$ in dB as shown in Figures 4 (j) and (k). The measurement of radiation pattern is performed in anechoic chamber and the normalized patterns in x - z and y - z planes at 5.8 GHz frequency are shown in Figure 4 (e) and during measurement port 2 is terminated with 50- Ω terminator and port 1 is excited. The difference between co- and cross-plane is observed at more than 20 dB in end-fire direction and stable radiations are observed. Figure 4 (d) represents the simulated and measured VSWR.

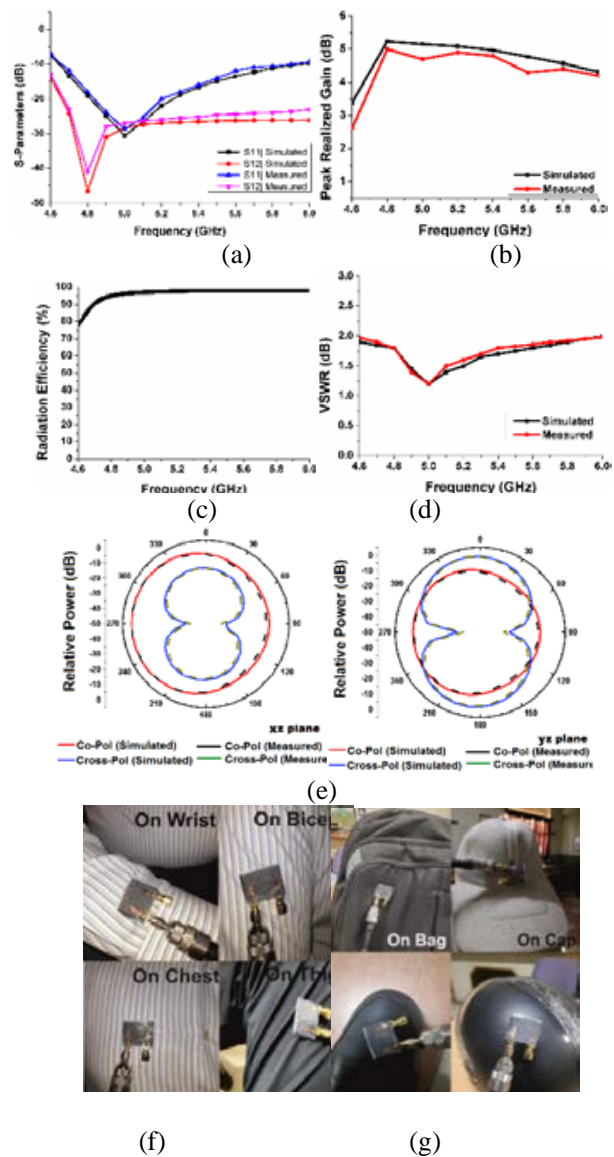


Fig. 4. Continued.

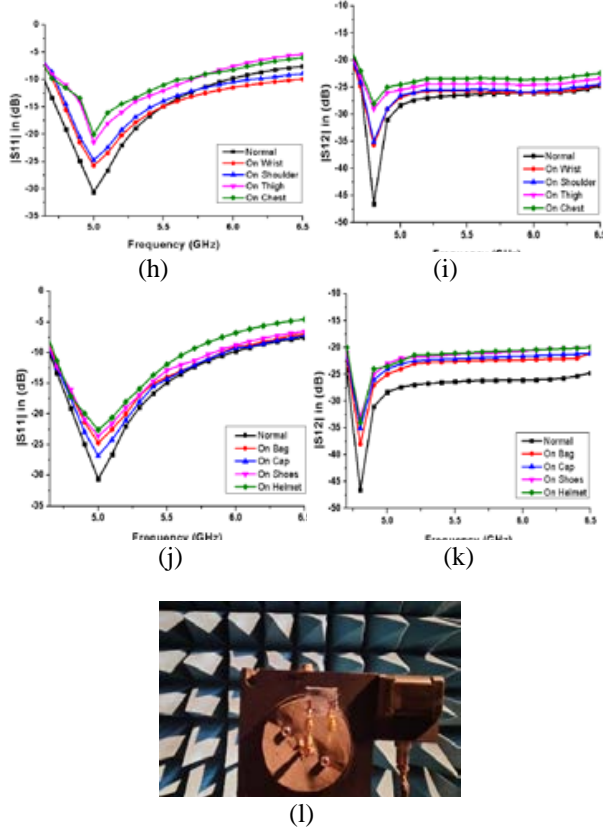


Fig. 4. Results (measured and simulated). (a) S -parameters (measured and simulated). (b) Realized gain (dB) (measured and simulated). (c) Radiation efficiency. (d) Simulated and measured VSWR. (e) Normalized radiation patterns in yz and xz planes at 5.8 GHz (measured and simulated). (f) Antenna placed on various body parts. (g) Antenna placed on different objects. (h) $|S_{11}|$ characteristics in dB on different body parts. (i) $|S_{12}|$ characteristics on different body parts. (j) $|S_{11}|$ in dB on different objects. (k) $|S_{12}|$ in dB on different objects. (l) Measurement of antenna in anechoic chamber.

VI. ANALYSIS OF ECC, CCL, TARC, AND DG

A. Formulation

For evaluating MIMO performance in diversity environment, certain parameters such as channel capacity loss (CCL), diversity gain (DG), total active reflection coefficient (TARC), and ECC are taken into consideration. All the parameters are measured using the eqn (6)–(9) [4]

$$\text{ECC} = \frac{|S_{11}^* S_{12} + S_{21}^* S_{22}|^2}{(1 - |S_{11}|^2 - |S_{21}|^2)(1 - |S_{22}|^2 - |S_{12}|^2)} \quad (6)$$

$$\text{DG} = 10\sqrt{1 - |\text{ECC}|^2}. \quad (7)$$

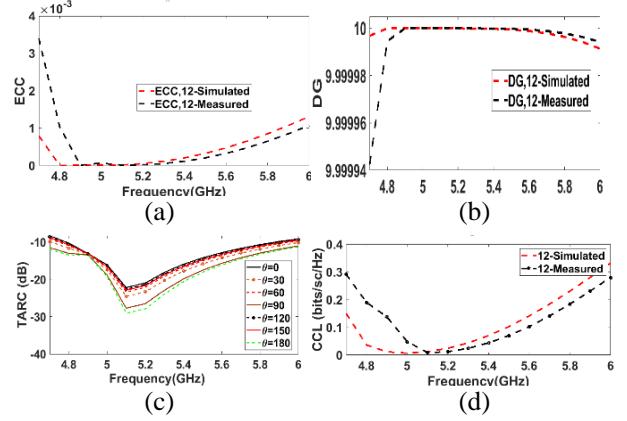


Fig. 5. MIMO parameters. (a) ECC. (b) Diversity gain. (c) TARC. (d) CCL.

$$\text{TARC} = \sqrt{|S_{11} + S_{12}e^{j\theta}|^2 + |S_{22} + S_{21}e^{j\theta}|^2} / \sqrt{2}, \quad (8)$$

where θ = phase angle between adjacent/diagonal ports.

$$\text{CCL} = -\log_2 \det(\psi^R), \quad (9)$$

and ψ = correlation matrix at the receiving end.

B. Explanation

ECC is an important parameter that represents the correlation between the antenna elements. ECC ranges from 0 to 1 where 0 represents no correlation and antennas are completely decoupled, whereas 1 indicates identical pattern and high coupling between antennas. A truly uncorrelated channel is highly unlikely; therefore, ECC, which is close to 0, is desirable, thereby exhibiting high diversity performance and DG [19]. ECC and DG are calculated from s -parameters and are extracted from eqn (6) and (7). The measured and simulated DG and ECC are illustrated in Figures 5 (b) and (a), in which ECC is less than 0.005 and DG is near 10 dB.

Radiating efficiency and bandwidth of MIMO are not accurately characterized by scattering matrix; therefore, TARC is used [20]. Two element antenna scattering parameters are used to extract the TARC from eqn (8). TARC with $\theta = 0^\circ, 30^\circ, 60^\circ, 90^\circ, 120^\circ, 150^\circ, \text{ and } 180^\circ$ is given in Figure 5 (c), where minimum variations are observed.

CCL is a measure of throughput of antenna, where the CCL value should practically be less than 0.4 bit/s/Hz [11]. For the whole operating band, which represents high throughput. The CCL is measured through eqn (9). The measured and simulated CCL is depicted in Figure 5 (d) and is lower than 0.4 bits/s/Hz.

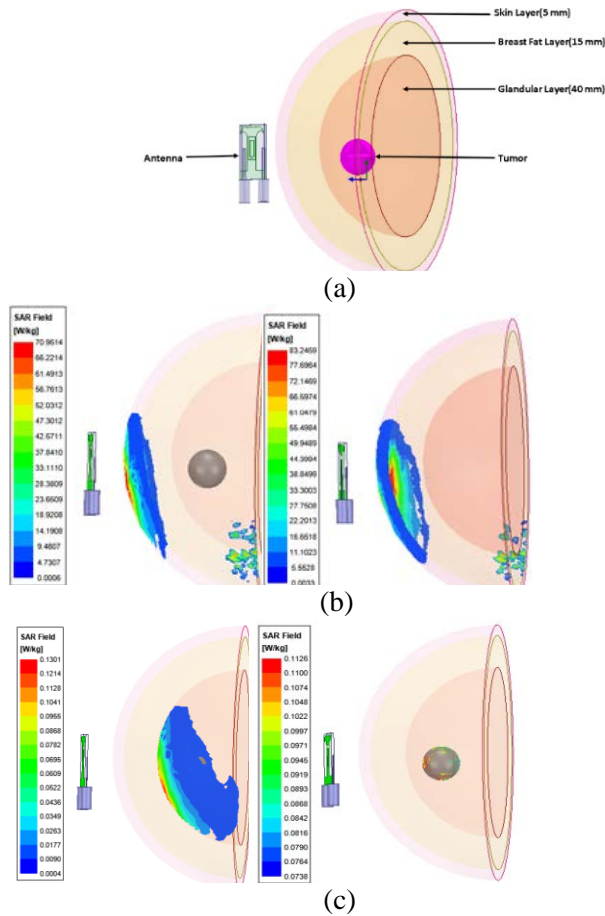


Fig. 6. (a) Breast model. (b) SAR of skin (without and with tumor). (c) SAR of glandular cell (with tumor) and SAR of tumor.

VII. TUMOR ANALYSIS ON FEMALE BREAST PHANTOM MODEL

Tumor in the female breast is very common in the soft glandular tissue, which is more vulnerable to developing malignant cells. In this paper, tumor analysis is investigated on female breast phantom model, with respect to SAR analysis.

The characteristics of tissue such as permittivity and permeability vary on occurrence of malignant (tumor) cell, thereby changing the SAR characteristics of the cell [32, 33]. Therefore, SAR analysis is the direct method for prediction of tumorous cells. A three-dimensional breast model (female) is illustrated in Figure 6 (a) for SAR analysis. The distance between breast model and antenna is 15 mm. The breast model with tumor size of 8 mm radius is composed of glandular tissue ($r = 40$ mm), breast fat ($r = 55$ mm), and outermost skin layer ($r = 60$ mm). The respective thickness of the layers is 40, 15, and 5 mm of glandular, breast fat, and skin layers [30, 32].

Table 2: SAR analysis (with and without tumor)

SAR (W/Kg) analysis at 5.8 GHz				
Tissue		With tumor	Without tumor	SAR diff.
Skin	Max	70.951	83.2459	12.2945
	Min	0.0006	0.0033	0.0027
Breast fat	Max	2.6118	2.6283	0.0165
	Min	0.0004	0.0003	0.0001
Glandular cell	Max	0.1301	0.1240	0.0061
	Min	0.0004	0.0003	0.0001
Tumor cell	Max	0.1126	–	–
	Min	0.0738	–	–

A. Detection of tumor

As the microwave field penetrates the tissue, the power is subsequently rejected through reflections and dissipation. Several tumor detection techniques are conventionally accounted [34, 35]. In the proposed method, tumor detection could be accomplished by using two different hypotheses. In the first hypothesis, the SAR value of the tumor and glandular tissue in the vicinity is analyzed for the detection of tumor cell; here, it is observed that the higher $SAR_{(avg)}$ value of the glandular tissue with tumor varies from 0.1301 to 0.0004 W/Kg, whereas SAR value of tumor tissue in glandular cell varies from 0.1126 to 0.0738 W/Kg, as shown in Figure 6 (c). The SAR difference denotes the presence of tumor, where the huge difference of minimum SAR value is detected in tumor cell and its neighboring glandular cell. In the second hypothesis, the difference in average SAR proves the presence of malignant (tumor) cell. It is observed that SAR values are decreased with the presence of tumor as given in Figure 6 (b). SAR difference (with and without tumor) is depicted in Table 2. In this investigation, the tumor analysis is observed effectively, which can be valuable for cancer detection and biomedical applications. In Table 3, the proposed two-port textile MIMO antenna is compared to the existing MIMO antenna, where proposed antenna is flexible and compact, based on textile material, with high isolation and have acceptable MIMO parameters, which can be applicable for WLAN and Wi-Fi communication in wearable applications.

VIII. CONCLUSION

A two-element MIMO antenna is designed and fabricated on denim textile as a substrate for 5G, WLAN frequency bands: Wi-Fi/WLAN (HIPERLAN, U-NII) (IEEE 802.11 a/h/j) working group as well as biomedical (ISM) band at 5.8 GHz. The isolation is achieved from defected ground decoupling structure such as horn-shape and CSRR. The horn-shaped ground disturbs the surface current and improves the isolation up to 5 dB, whereas

Table 3: Proposed MIMO antenna compared with existing MIMO antenna

Ref	Size (mm ²)	10 dB (GHz)	Isolation (dB)	Gain (dB)	Substrate	Flexibility	Isolation technology used	ECC
[2]	60 × 97	1.5–3.8, 4.1–6.1	15, 20	4	Jeans	Yes	Meander line structures	0.1
[4]	31 × 31	3.3–4.3	24	3.45	Jeans	Yes	Stubs and DGS, and orthogonal feed	0.2
[7]	140 × 70	2.33–2.5	26	4.7	Shieldit Textile	Yes	Conductive line	0.01
[9]	76 × 37	2.00–6.23	29.26	2.88	Felt	Yes	T-shaped stubs, ring-shaped slots, and meander line	0.01
[11]	80 × 170	3.4–3.6 and 3.9–4.5	20	6.8	FR4	No	T-shaped decoupling structure	0.3
[12]	18 × 44	3.3–3.65 and 4.8–5.5	18	5.93	FR4	No	Inverted T-shaped slot	0.002
[13]	55 × 35	2.4–9.0	18	9	Jeans	Yes	E-shaped stubs	0.06
[14]	71.7 × 50	3.24–3.05	19	4.7	FR4	No	Vertical and horizontal slotted ground	0.0035
[15]	35 × 30	3.11–5.15, 4.81–7.39	19, 21	NA	Jeans	Yes	Funnel-shaped DGS	0.18
[16]	30 × 50	3.14–9.73	32	2.7	Jeans	Yes	Neutralized ground	0.12
[17]	70 × 40	1.83–8	22	4	Jeans	Yes	I-shaped stubs	0.01
[21]	93 × 93	2.16–2.75	15	4.02	FR4	No	Square patch with circular chamfered corners	0.03
Proposed	24 × 28	4.65–5.97	20	4.57	Jeans	Yes	Horn-shaped defected coupling structure with CSRR	0.005

CSRR-shaped slot effectively diminishes the surface current and improves the isolation up to 27 dB. Overall, 20-dB isolation is achieved on the 10-dB impedance bandwidth of the proposed antenna that exists from 4.65 to 5.97 GHz; the antenna has simple decoupling structure and flexible substrate. The two-port MIMO antenna parameters are under the acceptable limit and antennas have minimum effect in s -parameter when analysis on bending was performed; this shows that the antenna is a suitable choice for wearable applications. Wi-Fi antennas are updated with MIMO technologies that allow group of devices to connect simultaneously to create efficient network and enhance speed and coverage. The MIMO antennas that are compact and integrated on fabrics could invariably be used for such applications in near future. The future technology holds easy-to-use and easy-to-fabricate antennas on other wearable textile substrates for 5G and 6G technologies that would be used in future. In future, more than two antenna elements would be designed for Internet of Things (IoT), sports, entertainment, and wearable technologies.

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