

# A Low-profile Wideband Pattern Reconfigurable Antenna with Metasurface

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**Abstract** – This paper presents a pattern reconfigurable antenna with low-profile and wide bandwidth. The antenna is composed of a patch layer, a metasurface (MS) layer, and a full ground plane. The radiation patch consists of a microstrip-fed square and three parasitic patches. The MS with  $4 \times 4$  units is added on the top of the patch layer to improve bandwidth as well as tune radiation pattern. Ten of the MS units are available to connect with the ground plane, each of which is loaded with a PIN diode to control the shorting state, providing 12 beam states with reconfigurable beams between  $\pm 5^\circ$  to  $\pm 15^\circ$  both in  $xoz$  and  $yoZ$  planes. The proposed antenna has been fabricated and measured. Measurement shows that the antenna has a wide impedance bandwidth of 4.02-5.72 GHz, a beam scanning range of  $-16^\circ$ - $15^\circ$  in  $xoz$  plane and  $-13^\circ$ - $15^\circ$  in  $yoZ$  plane, peak gain range of 4.94-6 dBi. With a planar shape of low profile and full ground plane, the antenna design is a good candidate to be applied in wireless communication systems with conductive surface.

**Index Terms** – 5G antenna, low-profile, metasurface (MS), pattern reconfigurable antenna, wideband antenna, WLAN antenna.

## I. INTRODUCTION

Pattern reconfigurable antennas have the capability to reconfigure radiation patterns to satisfy the requirements from communication systems of transmission efficiency improvement, transmission interference reduction and transmission quality enhancement. These kinds of antennas have found applications in the fields of vehicle communication, the Internet of Things, etc. [1–5].

The phased array antenna, although an effective approach for pattern reconfiguration, comes with bulk volume, high cost, and realizes beam pointing control through the integration of antenna elements, phase shifters, power splitters, and feed networks. Introducing

liquid crystal [6] or liquid metal [7] to tune material's permittivity or reshape the antenna's structure can also obtain pattern reconfiguration, however these methods involve difficulties of fast tuning as well as low efficiency.

Electrically controlling an antenna beam based on PIN diodes [8–23] offer advantages of fast modulation speed and compact structure which is desired in low-cost communication terminals. In these antennas, those with full ground plane [10–21] have virtues of good directivity and high gain. They are also immune to influence when mounted on conductive surfaces, such as vehicles, aircrafts, metallic walls, human bodies, etc. Therefore, antennas with full ground plane are more appealing in practical applications. Nevertheless, planar antennas with full ground plane come usually with narrow bandwidth [10–13]. Introducing an air gap [14–21] between ground plane and radiation patch is a commonly used solution to reduce the ground plane's influence. However increased height may bring instability problems and the inconvenience of being mounted on and conformal with the antenna supporter. Metasurface (MS) has been adopted in antenna configuration to improve bandwidth and reduce coupling with low profile [24–29], whereas pattern reconfiguration is unavailable in these antennas.

This paper aims to improve the bandwidth of pattern reconfigurable antenna considering low profile. A patch antenna with full ground plane is chosen as the driven element. Antenna bandwidth is improved by adding MS on top of the antenna. Some MS units are controlled by PIN diodes to connect/disconnect with the ground plane to obtain 12 reshaped patterns.

## II. ANTENNA CONFIGURATION AND OPERATION STATES

Figure 1 shows configuration of the proposed antenna. The antenna consists of three layers, a full ground plane at the bottom, radiation patches in the

middle layer, and a MS as the top layer. The radiation patches are composed of a square patch directly fed by a step shaped microstrip line and three parasitic patches. The MS with  $4 \times 4$  squares is adopted to obtain wideband impedance matching as well as pattern reconfiguration. Ten of the MS units are connected with the ground plane through via holes. Each via holes pad inside the MS unit is split with other parts of the unit by slits and loaded with a PIN diode to connect the via hole. Therefore, each unit can be controlled shorted/open with the ground plane to obtain pattern reconfiguration. Two FR4 boards each with a 1.5 mm thickness, a relative permittivity of 4.4 and a relative loss tangent value of 0.02 are used as substrates. The lumped components of each PIN diode's DC bias network are  $L1=L2=15$  nH,  $L3=2.2$  nH,  $R=200$   $\Omega$ , and  $C=10$  pF. The antenna dimensions are listed in Table 1. The PIN diodes used in this design are of Infineon BAR64-02V.

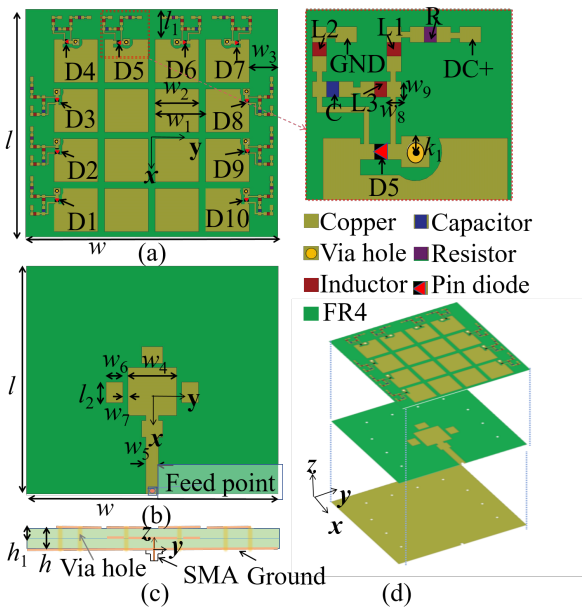


Fig. 1. Configuration of the proposed antenna: (a) top layer, (b) middle layer, (c) side view, and (d) 3D-view.

Table 1: Dimensions of the proposed antenna

Par.	Value (mm)	Par.	Value (mm)	Par.	Value (mm)
$w$	60	$l$	55	$h$	3
$w_1$	12	$l_1$	7.3	$h_1$	1.5
$w_2$	10.4	$l_2$	5	$k_1$	0.5
$w_3$	6.8	$w_6$	4	$w_9$	0.8
$w_4$	11.6	$w_7$	1.2		
$w_5$	3	$w_8$	0.83		

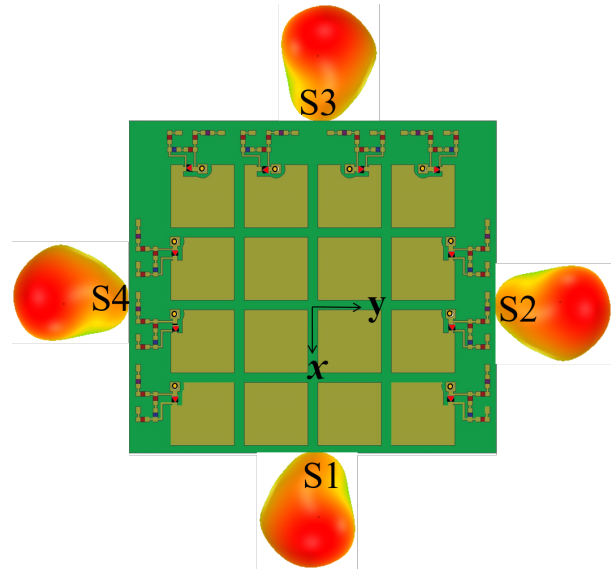


Fig. 2. Simulated 3-D radiation patterns for the proposed antenna at 5 GHz.

The proposed antenna can operate at 12 states with different beam directions listed in Table 2. In this table, the binary numbers in the second column refer to each PIN diode's working state: "1" means the PIN diode is turned on, and "0" means off. As shown in Table 2, the proposed antenna's beam can be steadily tuned from  $\pm 5^\circ$  to  $\pm 15^\circ$  with a step of  $5^\circ$ , both in  $xoz$  ( $\varphi=0^\circ$ ) and  $yoZ$  ( $\varphi=90^\circ$ ) planes. Figure 2 illustrates the radiation patterns of four typical operating states.

Table 2: Operating states of the proposed antenna at 5 GHz

State	D1-D10	Beam ( $\theta, \varphi$ )	Max Gain (dBi)
S1	0001111000	$\theta = +14^\circ$ in $xoz$ plane	7.41
S2	1111000000	$\theta = +15^\circ$ in $yoZ$ plane	6.36
S3	1100000011	$\theta = -14^\circ$ in $xoz$ plane	5.66
S4	0000001111	$\theta = -16^\circ$ in $yoZ$ plane	5.99
S5	0001001000	$\theta = +7^\circ$ in $xoz$ plane	7.08
S6	0101000000	$\theta = +9^\circ$ in $yoZ$ plane	6.47
S7	1000000001	$\theta = -8^\circ$ in $xoz$ plane	6.13
S8	0000001010	$\theta = -9^\circ$ in $yoZ$ plane	6.16
S9	0010000100	$\theta = +5^\circ$ in $xoz$ plane	6.70
S10	0110000000	$\theta = +5^\circ$ in $yoZ$ plane	6.55
S11	0100000010	$\theta = -5^\circ$ in $xoz$ plane	6.42
S12	0000000110	$\theta = -5^\circ$ in $yoZ$ plane	6.46

### III. ANTENNA DESIGN AND ANALYSIS

#### A. Antenna configuration design

Simulations are performed using the EM field simulator ANSYS High Frequency Simulation Software

(HFSS). The antenna design was conducted initially from bandwidth enhancement without considering beam reconfiguration. Figure 3 shows the design evolution with three reference antennas, and Fig. 4 gives simulated  $S_{11}$  of these antennas. As shown in Fig. 3 (a), ANT-1 is a traditional square-shaped patch antenna fed with a microstrip line. As shown in Fig. 4, ANT-1 excites the first resonance at 6.37 GHz which is traditionally a quarter wavelength resonance. By adding a MS layer on the top of ANT-1's patch layer, ANT-2's first resonance drops to 4.15 GHz, and a second resonance is excited at 4.91 GHz, which results in an improved bandwidth of 3.98-5.18 GHz. Based on ANT-2, three parasite patches are added around the driven patch, and the feedline is modified to a step shape forming ANT-3. As shown in Fig. 4, ANT-3 excites three resonances (4.53, 5.26, 5.67 GHz) below 6 GHz, resulting in wider bandwidth of 3.96-5.78 GHz. Figure 5 illustrates the 3-D radiation pattern of ANT-3 at 5 GHz. As shown, ANT-3 has a bore-sight maximum radiation pattern with a peak gain of 6.56 dBi.

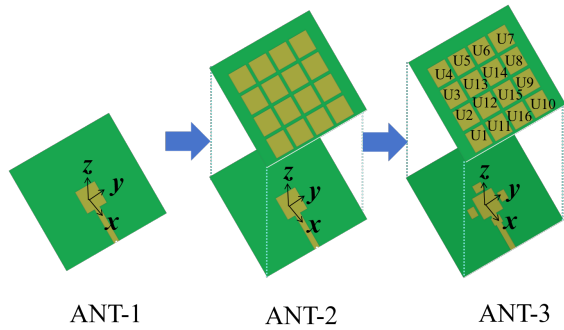


Fig. 3. Antenna configuration design evolution.

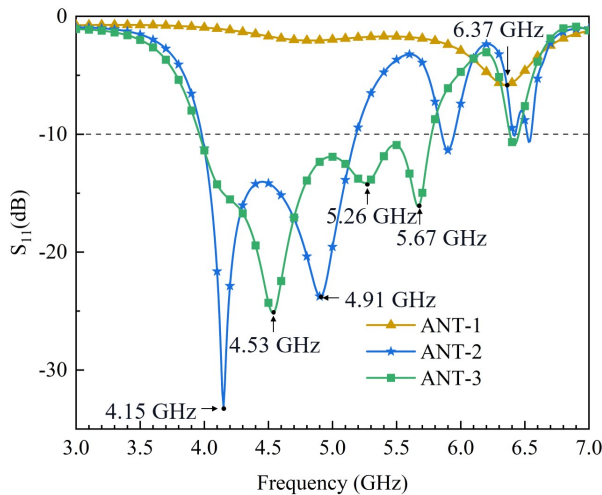


Fig. 4. Simulated  $S_{11}$  of reference antennas.

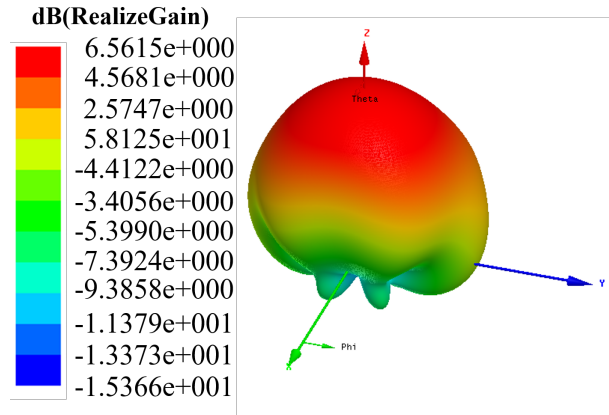


Fig. 5. Simulated 3-D radiation pattern of ANT-3 at 5 GHz.

**B. Mechanism of pattern reconfiguration**

Based on the configuration of ANT-3, each MS unit tried to connect with the ground plane through a via hole to obtain tilted radiation beam. The shorting position was arranged at the corner of each unit to reduce the influence on antenna bandwidth. Figure 6 illustrates radiation patterns and current distributions of ANT-3 with some MS units shorted. As shown in Fig. 6 (a), when only one unit (U1) is shorted, the current distributions on U1 becomes weaker than those on other units. This means that electromagnetic fields induced by U1 is bounded in the near region with little radiating to the far region which results in a tilted radiation pattern with main beam at  $\theta=5^\circ, \varphi=120^\circ$ . As shown in Fig. 6 (b), when four MS units at the left side (U1, U2, U3, and U4) are shorted, a larger tilted beam ( $\theta=15^\circ, \varphi=90^\circ$ ) is obtained. Similar approach is also presented in [30,31] which added shorting pins to the parasitic patches on the same layer with the driven patches. To the authors' best knowledge, it's the first time shorting pins were added on the MS patches which are in a different layer with the radiation patch to tune radiation patterns.

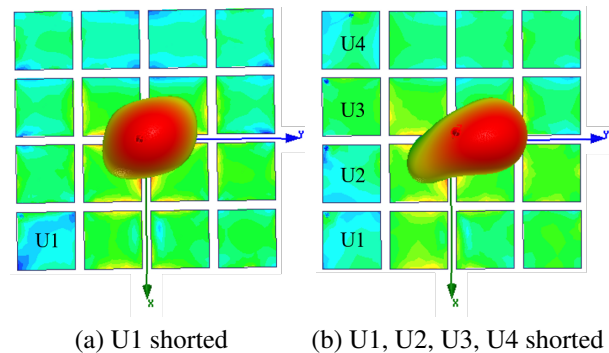


Fig. 6. Simulated current distributions and radiation patterns of ANT-3 with some MS units shorted.

Theoretically, each of the 16 units can be tuned with shorted/open with ground plane forming  $2^{16}$  reconfigurable patterns. Nevertheless, not all the patterns are reasonable for engineering application, and the convenience of installing PIN diodes and DC bias network in the design needs also be considered. Therefore, we chose the 10 units (U1-U10) located at three edges to form 12 working states with reconfigurable patterns.

### C. DC bias network and pattern reconfiguration realization

To electrically control each MS unit shorted/open with the ground plane, slits are etched around each via hole with loading a PIN diode. The DC bias network to power each PIN diode is shown in Fig. 1, which is similar with the one in [32]. The antenna's operation states are given in Table 2.

Figure 7 shows simulated  $S_{11}$  of the proposed antenna at six states (S1, S2, S5, S6, S9, S10). As shown, the proposed antenna has similar bandwidth with ANT-3 at these six states. The other six states (S3, S4, S7, S8, S11, S12) have similar  $S_{11}$  plots with the former ones which are not included in the figures. The common bandwidth for the 12 states is 3.96-5.78 GHz.

Figures 8 and 9 illustrate simulated patterns in  $xoz$  and  $yo z$  planes at 5 GHz, respectively. As shown in Fig. 8, the proposed antenna achieves titled beams in  $xoz$  plane at  $\theta=14^\circ$ ,  $\theta=-14^\circ$ ,  $\theta=+7^\circ$ ,  $\theta=-8^\circ$ ,  $\theta=+5^\circ$ , and  $\theta=-5^\circ$  at S1, S3, S5, S7, S9, and S11 states. Figure 9 shows that the antenna achieves titled beams in  $yo z$  plane at  $\theta=15^\circ$ ,  $\theta=-16^\circ$ ,  $\theta=+8^\circ$ ,  $\theta=-9^\circ$ ,  $\theta=+5^\circ$ , and  $\theta=-5^\circ$  at S2, S4, S6, S8, S10, and S12 states.

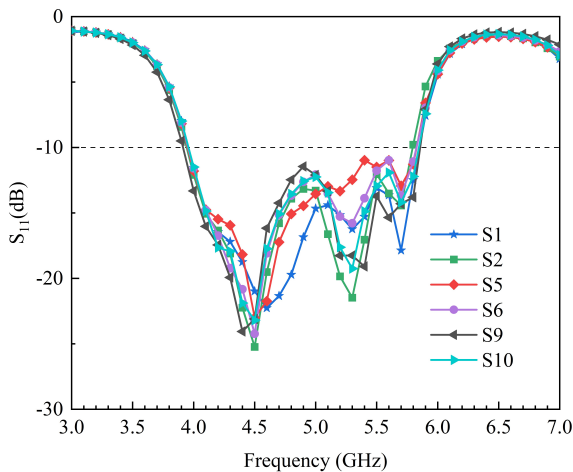


Fig. 7. Simulated  $S_{11}$  of the proposed antenna.

The positions of the PIN diodes and the shape of the slit have been optimized to reduce the influence on

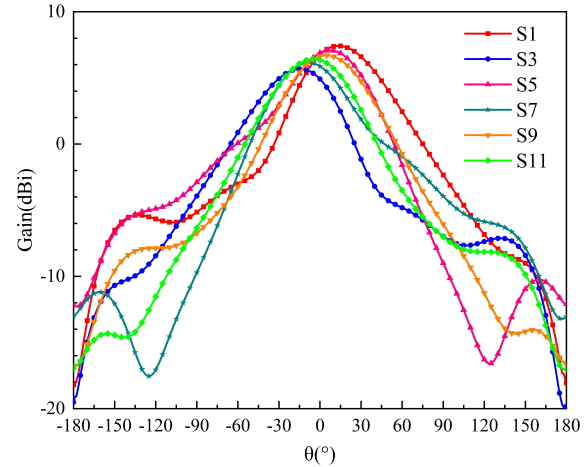


Fig. 8. Simulated radiation pattern in  $xoz$  plane at 5 GHz.

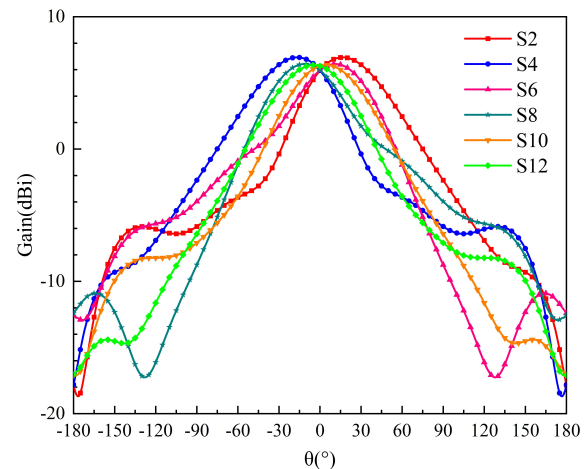


Fig. 9. Simulated radiation pattern in  $yo z$  plane at 5 GHz.

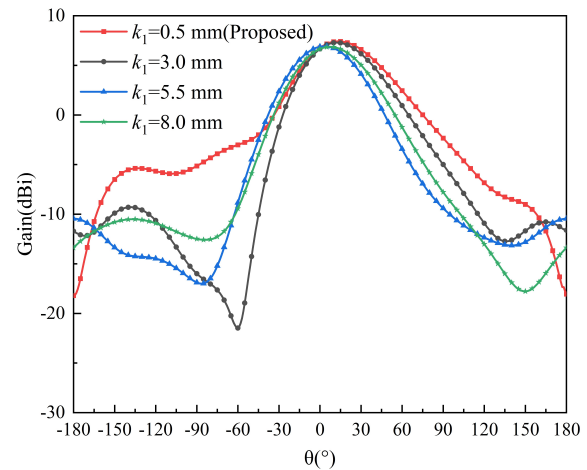


Fig. 10. Simulated radiation pattern in the  $xoz$  plane at State 1 varying with  $k_1$ .

antenna's pattern. Figure 10 shows simulated pattern in the  $xoz$  plane at state 1 varying with  $k_1$  (the position of each via hole). As shown, smaller  $k_1$  results in higher gain. The value of  $k_1$  is set as 0.5 mm to provide enough area to contain a via hole.

#### IV. RESULTS AND DISCUSSION

The proposed antenna has been fabricated and measured. Figure 11 shows a photograph of the fabricated antenna, in which each PIN diode is powered by a button battery assembled in a battery container.

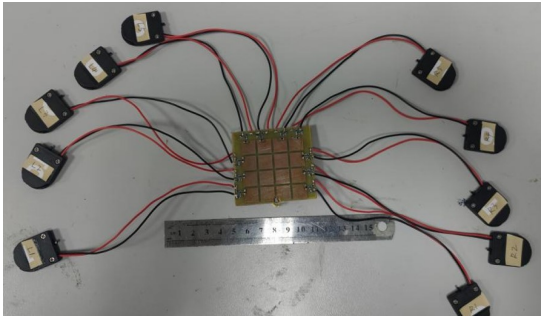


Fig. 11. Photograph of the fabricated antenna.

The proposed antenna was measured at S1, S2, S3, and S4 states. Measured  $S_{11}$  is illustrated in Fig. 12 which shows that the antenna has similar bandwidth in these four states, and a common bandwidth of 4.02–5.72 GHz. Radiation patterns of the four states at 4.8, 5, and 5.2 GHz are shown in Figs. 13–15, respectively. As shown in the figures, measurement agrees well with simulation. The proposed antenna achieves pattern reconfiguration both in  $xoz$  and  $yoZ$  planes. Table 3 lists measured

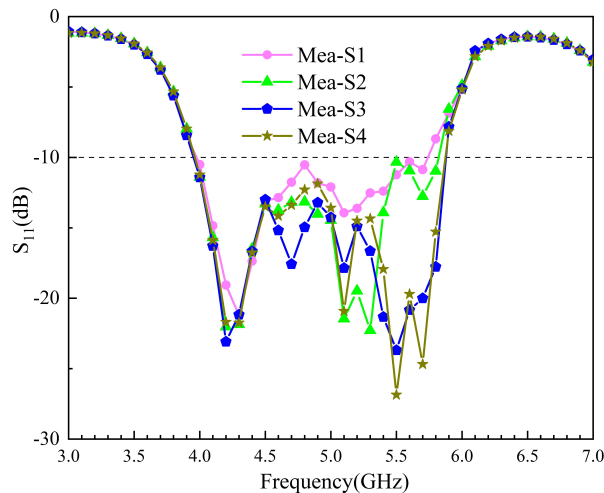


Fig. 12. Measured  $S_{11}$  of the proposed antenna.

peak gains and beams. As shown, the antenna realizes pattern reconfigurations ranging from  $-16^\circ$  to  $15^\circ$  in  $xoz$  plane, and  $-13^\circ$  to  $15^\circ$  in  $yoZ$  plane. Maximum gain in the working states ranges from 4.94 to 6 dBi.

Table 4 compares the performance of the antenna

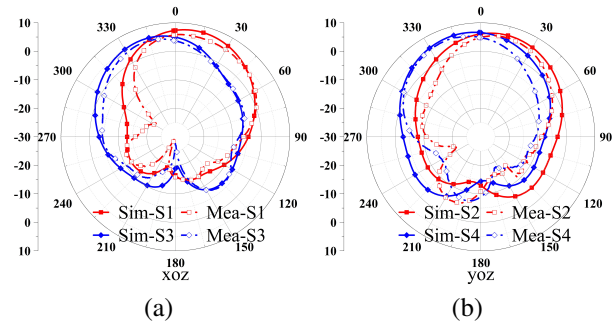


Fig. 13. Measured radiation pattern at 4.8 GHz.

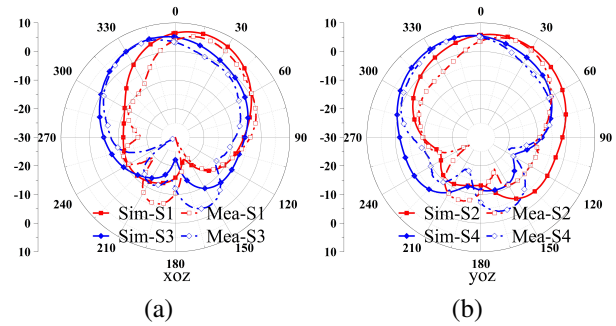


Fig. 14. Measured radiation pattern at 5.0 GHz.

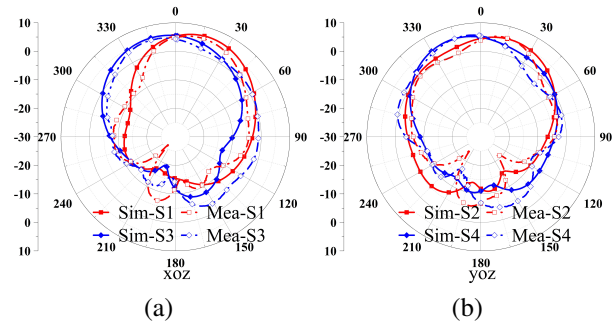


Fig. 15. Measured radiation pattern at 5.2 GHz.

Table 3: Measured peak beam and peak gain

	4.8 GHz		5 GHz		5.2 GHz	
	Beam ( $\theta, \varphi$ )	Gain (dBi)	Beam ( $\theta, \varphi$ )	Gain (dBi)	Beam ( $\theta, \varphi$ )	Gain (dBi)
S1	( $15^\circ, 0^\circ$ )	5.94	( $14^\circ, 0^\circ$ )	5.96	( $16^\circ, 0^\circ$ )	5.87
S2	( $15^\circ, 90^\circ$ )	5.91	( $15^\circ, 90^\circ$ )	5.88	( $16^\circ, 90^\circ$ )	5.82
S3	( $-16^\circ, 0^\circ$ )	4.94	( $-14^\circ, 0^\circ$ )	4.96	( $-15^\circ, 0^\circ$ )	5.01
S4	( $-13^\circ, 90^\circ$ )	6.00	( $-16^\circ, 90^\circ$ )	5.83	( $-14^\circ, 90^\circ$ )	5.62

Table 4: Comparison of the proposed antenna with published pattern-reconfigurable antennas

Ref.	BW (GHz)	BW (%)	Size ( $\lambda^3$ )	Peak Gain (dBi)	Number of PIN Diodes	Number of States	Beam Direction	Beam Range ( $^\circ$ )
[9]	3.54-4.46	23	$3 \times 1.24 \times 0.05$	7.67	18	5	1D	$\pm 55$
[10]	2.45-2.45	3.8	$0.45 \times 0.45 \times 0.02$	3.86	4	2	N/A	N/A
[11]	2.45-2.45	4.0	$1.7 \times 2 \times 0.007$	7.1	8	2	N/A	N/A
[13]	5.5-5.98	11.3	$1 \times 2 \times 0.06$	N/A	2	2	1D	$\pm 50$
Pro.	4.02-5.72	34	$1 \times 0.95 \times 0.05$	4.94-6	10	12	2D	$-16^\circ$ - $15^\circ$ in $xoz$ $-13^\circ$ - $15^\circ$ in $yoZ$

proposed in this paper with that of the beam-reconfigurable antennas in the references. As shown, the proposed antenna has virtues of smaller size, wider bandwidth and more tunable states with reconfigurable patterns.

## V. CONCLUSION

In this paper we have designed a pattern reconfigurable antenna based on a microstrip-fed patch antenna with full ground plane. A  $4 \times 4$  MS is adopted to improve bandwidth as well as realize pattern reconfiguration. Ten of the MS units are loaded with PIN diodes to control the connection/disconnection with the ground plane. DC bias network is arranged outside each MS unit and near its edge to maintain wide bandwidth and obtain good radiation pattern. By controlling each PIN diode's ON/OFF state, 12 states with different titled patterns are obtained. Antenna fabrication and measurement have been conducted to validate simulations. Measurement shows that the proposed antenna covers impedance bandwidth of 4.02-5.72 GHz and pattern reconfiguration bandwidth of 4.8-5.2 GHz. The antenna works at 12 pattern reconfiguration states ranging from  $-16^\circ$  to  $15^\circ$  in  $xoz$  and  $-13^\circ$  to  $15^\circ$  in  $yoZ$  plane. The proposed antenna has a small size  $1 \times 0.95 \times 0.05 \lambda^3$ . With a full ground plane and low profile, the proposed antenna is a good candidate applied in metallic vehicles.

$\lambda$  is the free space wavelength at the central operational frequency, Pro.=proposed.

## ACKNOWLEDGMENT

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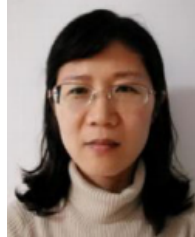
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