

High Impedance Surface Application to Dipole Antenna Design

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Abstract — in this paper, HIS (High Impedance Surface) are used, in order to verify their utilities; we have considered two different structures as a ground. The first is mushroom EBG (Electromagnetic Band Gap) structure which is composed of several patches with a ground connecting via, where the second is 2D metamaterial structure with resonant rings. Both the structures are investigated by simulation and compared at the frequency 12 GHz. The metamaterials proprieties are successfully verified around the resonant frequency.

Index Terms — Digital capacitance, EBG structures, metamaterials, negative index materials, wire antenna.

I. INTRODUCTION

The antennas manufacture requires a big precision in realization, because the dimensions of these circuits are of the same order of magnitude as the wave length. Considering imprecision factors due to the manufacture constraint, surface waves will be engendered; consequently, antenna performance will be influenced.

A special material is used to block surface waves known as metamaterial, it enhances significantly the antenna performance which is characterized by simultaneously negative values of the permeability and the permittivity [1]; it doesn't exist in natural state.

Metamaterials enhance significantly the antenna performance. They have interesting proprieties [2], it consists in stopping surface waves to propagate along the surface, there is no phase delay to be introduced to the progressive wave and the evanescent wave is amplified. Hence, we can say that both propagating and evanescent waves contribute to the resolution of the system and circuit's spatial frequency is restored. Therefore the wave behaves as there is no physical obstacle [3-4].

II. METAMATERIAL TRANSMISSION LINE THEORY

Figure 1 [5] shows a cell of metamaterial transmission line which is a combination of Right-Handed Transmission Line (RHTL) and Left-Handed

Transmission Line (LHTL). By applying the Kirchhoff law, it results:

$$\begin{cases} \frac{\partial v(x, t)}{\partial x} = Zi(x, t) = j \left(L_R \cdot \omega - \frac{1}{\omega \cdot C_L} \right) i(x, t), & (1) \\ \frac{\partial i(x, t)}{\partial x} = Yv(x, t) = j \left(C_R \cdot \omega - \frac{1}{\omega \cdot L_L} \right) v(x, t). & (2) \end{cases}$$

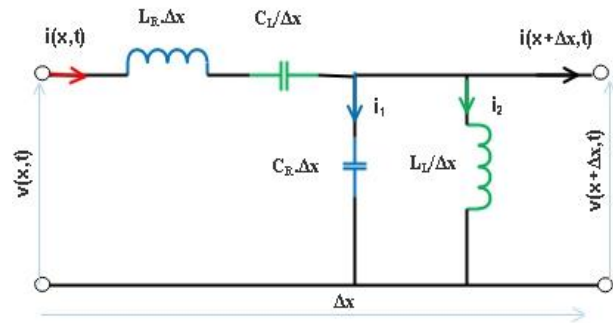


Fig. 1. Metamaterial transmission line cell model.

We solve simultaneously (1) and (2), we obtain the wave equations, for Voltage wave V:

$$\frac{\partial^2 v(x, t)}{\partial x^2} = -Z Y v(x, t) = -\gamma^2 v(x, t). \quad (3)$$

Where:

$$\gamma = \sqrt{Z Y} = \alpha + j\beta = \sqrt{-\omega^2 (L_R C_R + \frac{1}{(\omega^2 \sqrt{L_L C_L})^2}) - \frac{L_R C_L + L_L C_R}{(\omega \sqrt{L_L C_L})^2}}. \quad (4)$$

We can introduce the RH resonant frequency: $\omega_R = \frac{1}{\sqrt{L_R C_R}}$. And LH resonant frequency $\omega_L = \frac{1}{\sqrt{L_L C_L}}$, it results:

$$\gamma = j \sqrt{(\omega / \omega_R)^2 + (\omega_L / \omega)^2} - k \omega_L^2. \quad (5)$$

Equation (5) describes all the behaviors of the metamaterial transmission line.

Figure 2 shows the graph of the complex propagation constant. Where $A = \max(\omega_s, \omega_p)$, $B = \min(\omega_s, \omega_p)$ and $C = \omega_F$, ω_s , ω_p and ω_F are respectively the series, shunt resonance frequencies and maximum attenuation frequency [5].

We consider Fig. 2, if $\omega < \min(\omega_s, \omega_p)$, the phase velocity (slope of the line segment from origin to curve) and group velocity (slope of the curve) have opposite sign (they are antiparallel) which means that the transmission line is left-handed and that β is therefore negative.

If we apply Maxwell equations and use (1) and (2), it results:

$$\begin{cases} \mu(\omega) = L_R - \frac{1}{\omega^2 C_L}, & (6) \\ \varepsilon(\omega) = C_R - \frac{1}{\omega^2 L_L}. & (7) \end{cases}$$

When $\omega \ll \min(\omega_s, \omega_p)$, (6) and (7) become:

$$\begin{cases} \mu(\omega) = -1/\omega^2 C_L < 0 \\ \varepsilon(\omega) = -1/\omega^2 L_L < 0 \end{cases} \text{Left-Handed Transmission Line.}$$

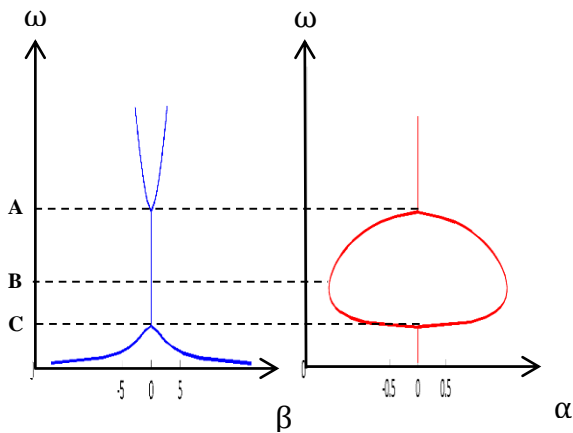


Fig. 2. Complex propagation constant vs. frequency

III. SIMPLE DIPOLE ANTENNA RESPONSE

Figure 3 shows the radiation pattern of dipole antenna in free space. In horizontal plane (3.B), when viewed from above, the pattern exhibits two lobes which represent the omnidirectional characteristic of the dipole antenna (bidirectional radiation).

When a dipole antenna is installed close to the earth's surface, the pattern radiation is attenuated because of the reflection from the surface [6]. In the ideal case, the gain of the dipole antenna doesn't exceed 3 dB as shown on Fig. 4.

IV. MODELS AND DIMENSIONS

In order to investigate the performance of the dipole antenna, it will be installed close to different surfaces and each structure will be also optimized in order to seek the best results.

A. Dipole above a perfect electric conductor (PEC)

The most simple structure is a ground plane placed under the dipole antenna (27.5X27.5 mm) of distance $h_{dist} = 1.925$ mm functions as reflector as shown on Fig. 5.

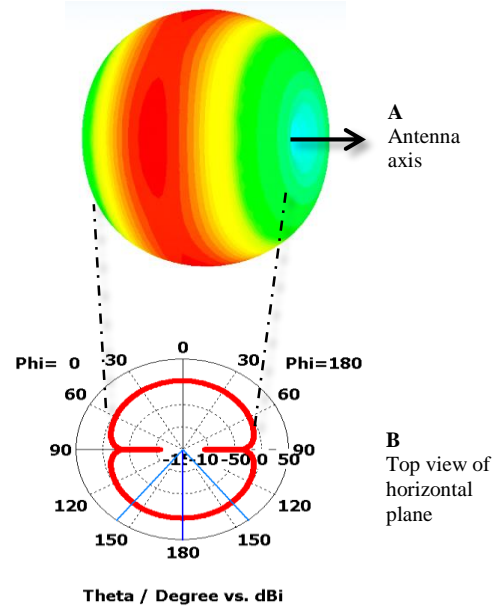


Fig. 3. Idealized dipole radiation pattern.

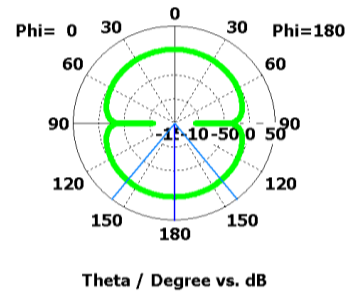


Fig. 4. Dipole radiation diagram of the gain at 12 GHz.

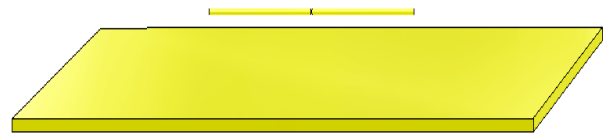


Fig. 5. Dipole antenna above a reflector.

B. Dipole above EBG substrate (mushroom)

The second model is the dipole antenna placed above EBG substrate of distance $h_{dip} = 0.02\lambda$. It is composed of several patches of side width $w = 0.12\lambda$, gap width $g = 0.02\lambda$, substrate thickness $h = 0.04\lambda$ and via hole of ray $r = 0.005\lambda$.

We have considered the following parameters as: dipole length $L = 0.452\lambda$ and dielectric constant $\epsilon_r = 2.17$ for the frequency 12 GHz (red graph in Fig. 10), the dipole length $L = 0.457\lambda$ and dielectric constant $\epsilon_r = 2.2$ for the frequency 12.228 GHz (green graph in Fig. 10). Figure 6 illustrates the model.

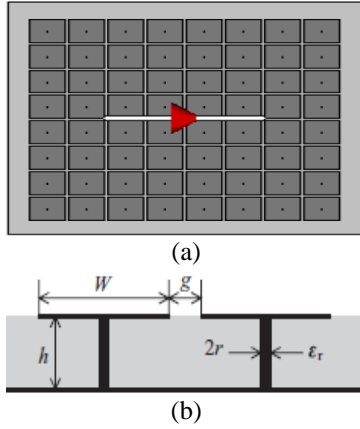


Fig. 6. (a) Dipole antenna above mushroom structure, and (b) parameters of mushroom cells.

C. Dipole antenna above 2D structure substrate with digital capacitors and rings

The third model is the dipole antenna placed above substrate of distance $h_{dip} = 0.02\lambda$, permittivity $\epsilon_r = 2.2$ and thickness $h = 1.25$ mm. It is composed of several patches of width $w_{patch} = 0.084\lambda$, seven digits digital capacitors of parameters $w_{digit} = 0.0084\lambda$ and rings with parameters: $r_{ring} = 0.08\lambda$ [7], $a = 0.007\lambda$, the space between rings $g = 0.02\lambda$ and via hole of ray $r = 0.005\lambda$.

We have considered the digit length of the digital capacitor (L_{digit}) and the dipole length (L) as follows:

$$L_{digit} = \lambda/4 \quad \text{and} \quad L = 0.41\lambda;$$

for the frequency 12 GHz (red graph in Fig. 12):

$$L_{digit} = \lambda/5 \quad \text{and} \quad L = 0.42\lambda;$$

for the frequency 11.772 GHz (green graph in Fig. 12).

Figure 8 illustrates the model, where the digital capacitor as shown on Fig. 7 can be calculated by the following formula [8]:

$$C \left(\frac{pF}{\mu m} \right) = (\epsilon_r + 1)l[(N - 3)A_1 + A_2]. \quad (8)$$

Such as:

$$A_1 = 4.409 \tanh [0.55(h/W)^{0.45}]10^{-6}, \quad (9.a)$$

$$A_2 = 9.92 \tanh [0.52(h/W)^{0.5}]10^{-6}. \quad (9.b)$$

Where $W = S = S'$, N is the number of digits.

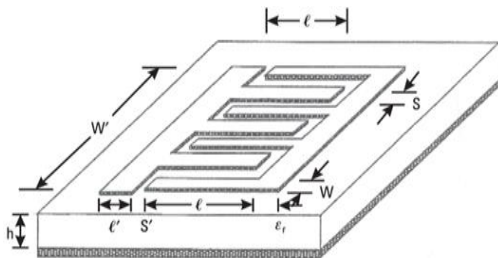


Fig. 7. Seven digits of the digital capacitor.

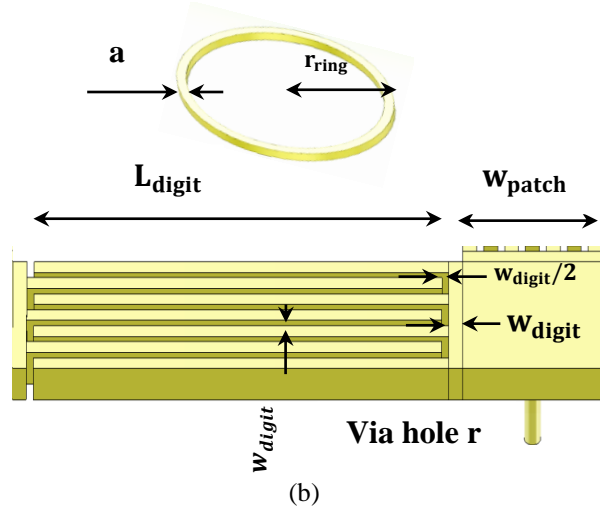
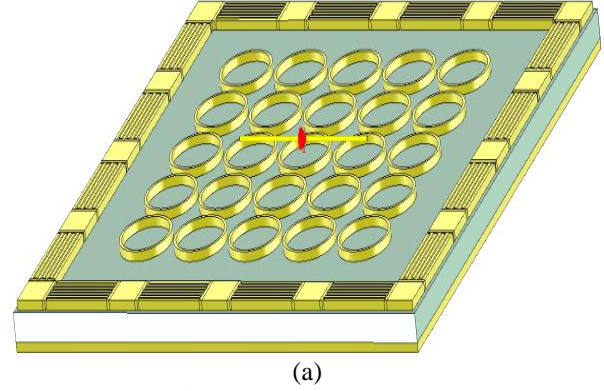


Fig. 8. 2D structure with digital capacitor and rings: (a) structure and (b) parameters.

V. RESULTS

The return loss of the first model as shown on Fig. 9 below doesn't satisfy the minimum attenuation, it can't be used as a ground.

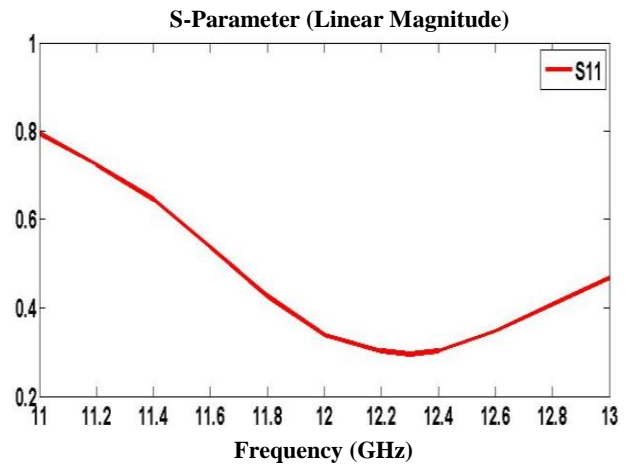


Fig. 9. Return loss vs. frequency of the dipole above PEC ground.

Figure 10 shows the graph of the reflection coefficient dipole antenna above mushroom structure. Two different graphs appear: we have considered the dipole length $L = 0.452\lambda$ and $\epsilon_r = 2.17$ for the red graph, the dipole length $L = 0.457\lambda$ and $\epsilon_r = 2.2$ for the green graph.

From the curve it's clear that the antenna at 12.228 GHz reaches a perfect resonance, it has the minimum value of the reflection coefficient -41.39 dB compared to 12 GHz operating frequency which has less reflection -26.45 dB.

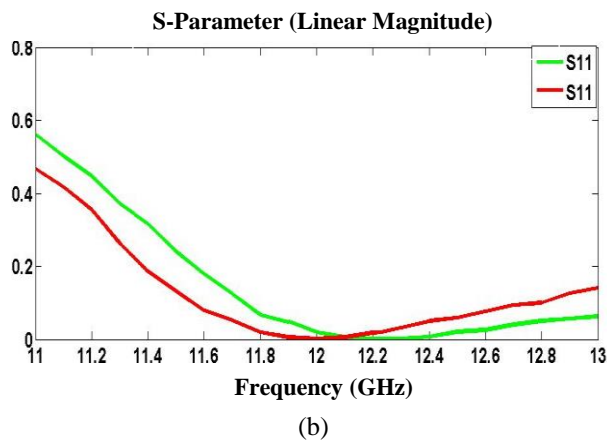
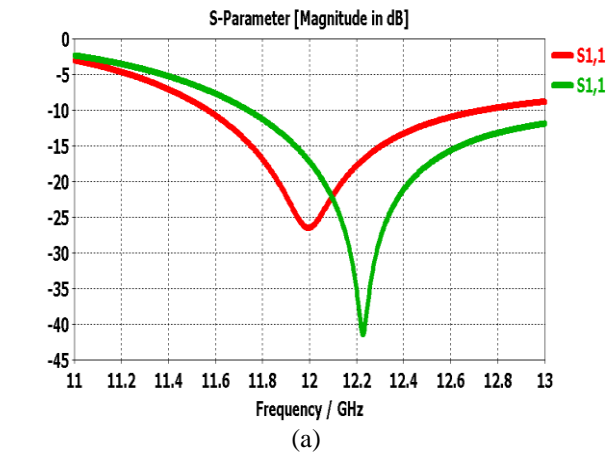


Fig. 10. Dipole mushroom return loss for 12 GHz operating frequency and around: (a) magnitude in dB and (b) linear magnitude.

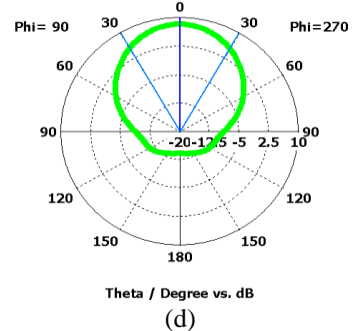
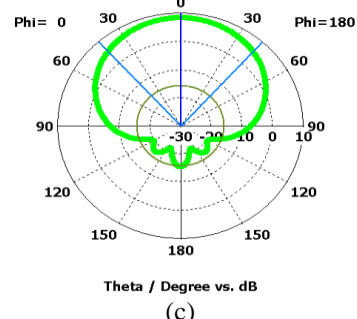
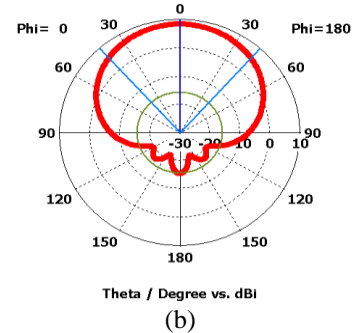
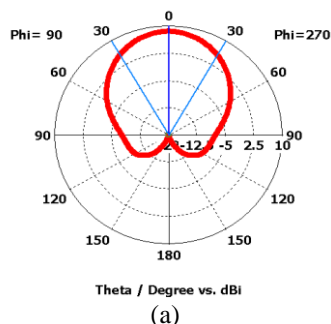


Fig. 11. Dipole mushroom parameters: (a) directivity at 12.228 GHz, (b) directivity at 12 GHz, (c) gain at 12 GHz, and (d) gain at 12.228 GHz.

Figure 11 shows the different parameters of the dipole mushroom structure, the graphs show that the gains are closely similar at 12 GHz and 12.228 GHz, they reach 8.3 dB, but the structure is more directive at 12.228 GHz, 59.8 deg. compared to 83.5 deg. at 12 GHz.

Figure 12 shows the graph of the reflection coefficient dipole antenna above 2D structure with digital capacitors and rings. Two different graphs appear: we have considered $L_{digit} = \lambda/4$ and the dipole length $L = 0.41\lambda$ for the red graph, $L_{digit} = \lambda/5$ and the dipole length $L = 0.42\lambda$ for the green graph.

Compared to the mushroom structure, we have more reflection at 12 GHz and also around the resonant frequency: -30 dB at 12 GHz and -45 dB at 11.772 GHz.

combined resonators with 2D metamaterial make the circuit original compared to the classical mushroom.

The results are obtained by using CST which is based on one of the most popular numerical method for the solution of electromagnetic problems (FDTD) [9].

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