

Experimental Analysis on the Performance and Characteristics of Compact Solar Refrigeration System

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ABSTRACT

This article focuses on the experimental analysis of fabricated Compact Solar Refrigeration System (CSRS) for small capacity cooling applications operating with water as refrigerant and lithium bromide as absorbent. Micro nozzles are introduced in the evaporator and in the absorber to shower the operational fluids in the system with the objective of increasing the heat transfer with effective absorption in the evaporator and absorber respectively. Modelling and performance analysis of the CSRS has done the influence of source temperatures and other operating parameters on the performance of systems fitted with micro nozzles. It appears that the coefficient of performance in CSRS has been improved from 0.3 to 0.6, since the heat transfer rate is improved in evaporator.

Keywords: Compact Solar Refrigeration System, Li-Br, Micro nozzles.

INTRODUCTION

The energy demand on the cooling application is considerably increasing in domestic and industrial applications and also scarcities of non-renewable energy sources are increasing. The solution for meeting the demand is renewable energy sources like solar energy, bio-fuel, etc... and recovery of wasted heat. Lot of work have been initiated in using

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renewable energy for the cooling applications which is available in clean form and in plenty.

Solar energy is used in the refrigeration systems in two ways, one is by solar PV system which converts solar energy to electric energy which can be used in Vapour Compression Refrigeration System and the second method is by using Solar Collecting system which converts solar energy to heat energy which can be used in Vapour Absorption Refrigeration System.

Solar Absorption Refrigeration System

In general, Vapour Absorption Refrigeration Systems (VARs) use low grade/temperature energy and the alternative option is using solar energy. VARs requires a robust construction compared to the Vapour Compression Refrigeration System for the same cooling load. The high capacity Vapour Absorption Refrigeration Systems uses fire wood, coal, diesel etc. [2]. A solar powered VARs operates by directly harnessing solar energy for the cooling purpose. Previous researchers have shown that the vapour absorption refrigeration systems generally offer smaller Coefficient of Performance (COP) and are commonly used for high capacity cooling loads [1] using coal or diesel etc., that are non-renewable and emit harmful greenhouse effects.

Compact Solar Refrigeration System

The absorption refrigeration systems utilising solar energy with smaller capacity are called Compact Solar Refrigeration Systems (CSRS). CSRS can be used in wide real life applications like cooling systems for travel, in rural areas and remote cold storages. CSRS receives the solar energy through the solar collectors for operation.

Performance Analysis of CSRS

The coefficient of performance (COP) of the solar refrigeration system generally depends on the performances of solar collector, generator, evaporator, and condenser and also depends on the pair of working fluid combinations which is used in the system. In the past five decades many efforts in these directions have been made and reports have been submitted on the performance analysis of solar refrigeration systems [3, 4]. Generator performance of the system is purely reliant on the heat source supplied to it [5]. The heat source for the SARS is solar energy through the solar collector. This solar collector converts the solar energy to heat

energy which is then input into the SARS in the form of hot water. The temperature of the hot water depends on the performance of the solar collector. The review on the solar collector shows that the performance of the solar collectors mainly depends on the shape of the collector [6]. The different types and shapes of solar collector give the different heat outputs. The COP of the SARS also depends on the condenser performance and the review indicates that the higher the effectiveness of the condenser the correspondingly higher the performance of the system [7].

Working Fluids in CSRS

The other important factor to be considered for the performance of the SARS system is the pair of refrigerant and absorbent working fluids. The working fluid pairs which are used in the SARS should be carefully planned for an eco-friendly and good thermo mechanical properties. The study on the performance of various pairs of refrigerant and absorbent indicates that a water and lithium bromide combination suits for small capacity applications and the pair has the advantage of utilizing the low level heat energy and is also considered eco-friendly [9, 10]. Also, various studies show that absorption refrigeration systems perform well for higher capacities outputs compared to the smaller capacities [11, 12].

CSRS with Micro Nozzles

This review provides a need for further studies on small capacity absorption refrigeration systems with better performance [8]. In this work copper tubes are attached with micro nozzles for spraying working fluids on the overheat exchanger coils available in the CSRS. This results in the increase of heat transfer in the evaporator and absorber by 20% which influences the COP of the system from 0.1 to 0.5. The performance of the system was analysed with different temperatures of hot water supplied to the generator. Temperature variation happened due to the solar insolation.

CONSTRUCTION OF CSRS

Construction of the CSRS is shown in the Figure 1. It contains two vessels connected by tubes. The upper vessel is divided into two compartments by a short wall where the right side compartment a strong solution sprayed over the hot water tubes receiving the heat energy

from the solar collector. The strong solution will absorb heat from the hot water, thereby the refrigerant in the strong solution evaporates and will pass over the condenser tubes which are in the left side compartment of the same vessel. The cold water circulated in the condenser coil takes off the heat from the refrigerant vapour, thus condensing the vapour into liquid.

In the lower vessel, the condensed refrigerant will be sprayed on evaporator coils. As the refrigerant evaporates, it takes the heat from the fluid circulated in the evaporator coils and the cooling effect is obtained. The evaporated refrigerant vapour will be absorbed by the absorbent which is available in the next compartment of the same vessel and forms the strong solution. Pumps are used to circulate the fluids between the upper and lower vessels. The performance of the CSRS is obtained by evaluating the coefficient of performance, which is the ratio of the cooling obtained in the evaporator to the heat supplied to the generator. The power input for the pumps is negligible relative to the heat input at the generator, therefore the working of the pump is often neglected during analysis.

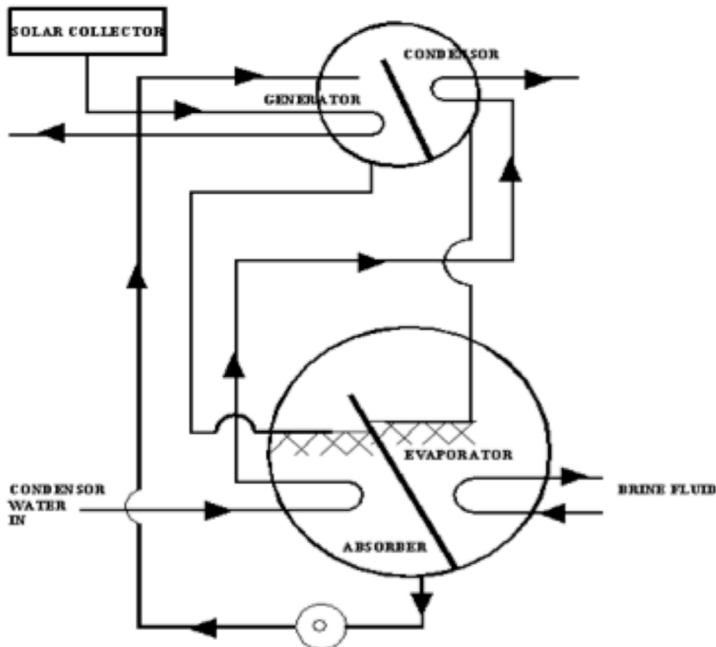


Figure 1. Layout of CSRS

PROBLEM FORMULATION

A mathematical model is used to analyse the performance of the CSRS. This model shows the relationship between the following parameters, namely:

- Heat removed in the evaporator
- Heat supplied in the generator
- Heat removed in the condenser
- Temperatures of the brine at inlet and outlet
- Temperatures of the generator fluid at inlet and outlet and
- Condenser fluid temperatures at inlet and outlet.

The mathematical model is formulated using the second law of thermodynamics along with heat, mass, and the energy balances. First, Equation 1 reveals the relationship between the heat generated in the generator, heat removed in the evaporator and with the absolute temperatures

$$\frac{Q_g}{T_g} + \frac{Q_e}{T_e} = \frac{Q_c}{T_c} \quad (1)$$

Next, Equation 2 is to find out the Coefficient of Performance (COP) using the relationship between the heat generated in the generator, heat removed in the evaporator and the absolute temperatures.

$$CPO = \left(\frac{T_e}{T_c - T_e} \right) \left(\frac{T_g - T_c}{T_g} \right) \quad (2)$$

Where,

Q_e = Heat removed in the brine evaporator in Watts

Q_g = Heat supplied to the generator in Watts

Q_c = Heat removed from the refrigerant at the condenser in Watts

T_g = Temperature at which heat (Q_g) is given to the generator in °C

T_c = Temperature at which heat (Q_c) is discharged to atmosphere in °C

T_e = Temperature at which heat (Q_e) is absorbed in the evaporator in °C

Equation 3 is used to find the experimental COP of the CSRS using the relationship between the heat removed from the brine and heat supplied at the generator.

$$\text{COP} = \frac{Q_e}{Q_g} \quad (3)$$

$$Q_g = mc_p (T_{hi} - T_{ho}) \text{ in Watts} \quad (4)$$

$$Q_c = mc_p (T_{ei} - T_{eo}) \text{ in Watts} \quad (5)$$

Where,

m = Mass flow of hot water from the solar collector in Kg/Sec

c_p = Specific heat of the hot water in $W/kg^\circ C$

T_{hi} = Temperature of the hot water at inlet of the generator $^\circ C$

T_{ho} = Temperature of the hot water at the outlet of the generator $^\circ C$

T_{ei} = Temperature of the brine inlet in the evaporator $^\circ C$

T_{eo} = Temperature of the brine at outlet of the evaporator $^\circ C$

EXPERIMENTAL FACILITY

The CSRS is designed with the consideration of good mechanical and chemical behaviour with suitable piping and vessel materials fabricated with lot of care. All the heat transfer equipment like evaporator, condenser, and generator cooling coils in the absorber were carefully tested and proved for the leak proof. Micro nozzles are introduced in the spray pipes to enhance the heat transfer rate in the evaporator and effective absorption in the absorber. Care is taken much in fabricating and evacuating the setup. After fabricating the equipment the charging of the working fluids is done. Then leak test is performed on the system followed by load test for mechanical and chemical stability. The fabricated experimental setup is shown in the Figure 2.

Composition of Working Fluids in CSRS

The working fluids used in the CSRS are Lithium Bromide (LiBr) as absorbent and the properties of the LiBr are as follows:

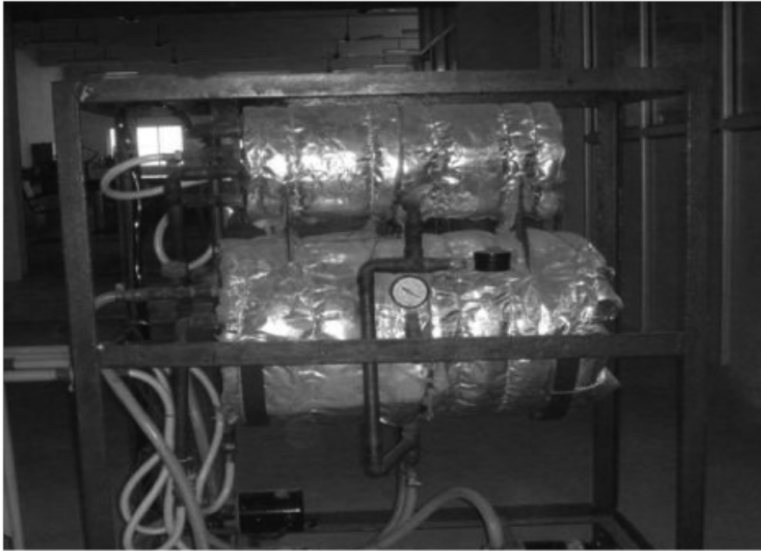


Figure 2. Experimental set up of the compact solar refrigeration system

Molecular Weight:	86.85
Composition:	lithium 7.99% bromide 92%
Specific Gravity:	3.46 at 25°C
Melting Point:	549°C and
Boiling Point:	1265°C at atmospheric pressure conditions

Water (H_2O) is taken as refrigerant. This is pure and free of contaminants. LiBr is corrosive in the presence of air so, corrosion inhibitors, such as Lithium Chromate, are charged into the system to retard corrosion. Octyl Alcohol (2-Ethyl 1-Hexanol) is added as additive to increase absorption effect of the absorbent.

Specification of the Compact Solar Refrigerator

The operating parameters of the compact solar refrigeration system for the performance analysis ratings are listed in Table 1.

The experiment was conducted with different generator inputs at different time intervals. The parameter data related to generator condenser and evaporator performance during the experiment are given in Table 2.

Table 1. Specification of CSRS

Serial No.	Description	Rating
1	Mass flow in generator	0.00467 kg/s
2	Generator inlet temperature	75 – 93 °C
3	Mass flow in Condenser	0.006 kg/s
4	Condenser inlet temperature	25 – 35 °C
5	Mass flow in Evaporator	0.005 kg/s
6	Evaporator outlet temperature	19 – 22 °C

Table 2. Parameters obtained in the experiment

Serial No	Time (min)	Generator			Condenser		Evaporator			
		Temperature (°C)		FlowRate (ml/min)	Temperature (°C)		FlowRate (ml/min)	Temperature (°C)		
		Inlet	Outlet		Inlet	Outlet		Inlet	Outlet	Out let (after fitting Nozzle)
1	90	75	50.0	280	25	36.0	360	32.0	22.0	17.0
2	105	78	53.0	280	25	36.0	360	33.0	21.0	16.5
3	120	80	55.0	280	25	36.5	360	33.0	20.5	17.5
4	135	83	56.0	280	26	36.5	360	33.5	20.0	17.5
5	150	85	57.0	280	28	37.0	360	33.5	20.0	15.5
6	165	87	58.0	280	29	37.0	360	34.0	20.0	15.5
7	180	88	58.5	280	29	37.5	360	34.5	20.0	15.5
8	195	89	59.0	280	30	37.5	360	34.5	19.5	16.0
9	210	92	61.0	280	33	37.5	360	34.0	19.0	16.0
10	225	93	63.0	280	35	37.5	360	34.0	19.0	16.5

RESULTS AND DISCUSSION

The recorded experimental values are used in formulated models to analyse the performance of CSRS. The temperature variations with respect to time for the different components of the CSRS are given in Figure 3. It is indicated that the generator input temperature is found

to be increased with respect to time, condenser outlet temperature and evaporator inlet. Temperature is not having significant variation with respect to time. Also, it is identified that the expected cooling temperature is obtained constantly with respect to time in the experimental system.

The variation of experimental COP with respect to the brine outlet temperature is represented in Figure 4. COP is 0.6 at low temperatures and is not varying for small increase in the outlet temperature of the brine solution.

The heat removed in the evaporator with respect to the brine outlet temperature is shown in the Figure 5. The heat removal rate is considerably decreasing with respect to the increase in the brine outlet temperature. It clearly indicates that if the load on the system increases the performance is decreasing.

The variation in theoretical COP and the experimental COP with respect to the brine outlet temperature is given in Figure 6. The theoretical performance and experimental performance of the system have negligible deviation for the low brine outlet temperature and there is significant variation for the increase in the temperature of the brine outlet temperature. The maximum variation is 0.15 is indicating that the theoretical COP is increasing and the experimental value is decreasing with respect to the rise in the brine outlet temperature.

The effect of nozzles with respect to the performance is indicated in the Figure 7. It shows the performance of the CSRS system is improved by increasing the heat transfer rate in the evaporator, raising the COP from 0.3 to 0.6.

CONCLUSION

The experimental results and analysis show that the compact solar refrigeration system performs well for the low cooling load and is well suited for the small capacities. The hot water inlet temperature in the generator influences the CSRS performance and the optimum hot water inlet temperature of the generator is 95°C. The temperature reduction achieved in the brine of the evaporator is from 10°C to 15°C. Introduction of nozzles in the evaporator improves the performance of the system. In future this system with nozzles can be used with the heat resources like bio-gas in domestic plants and burning of sugar cane bagasse.

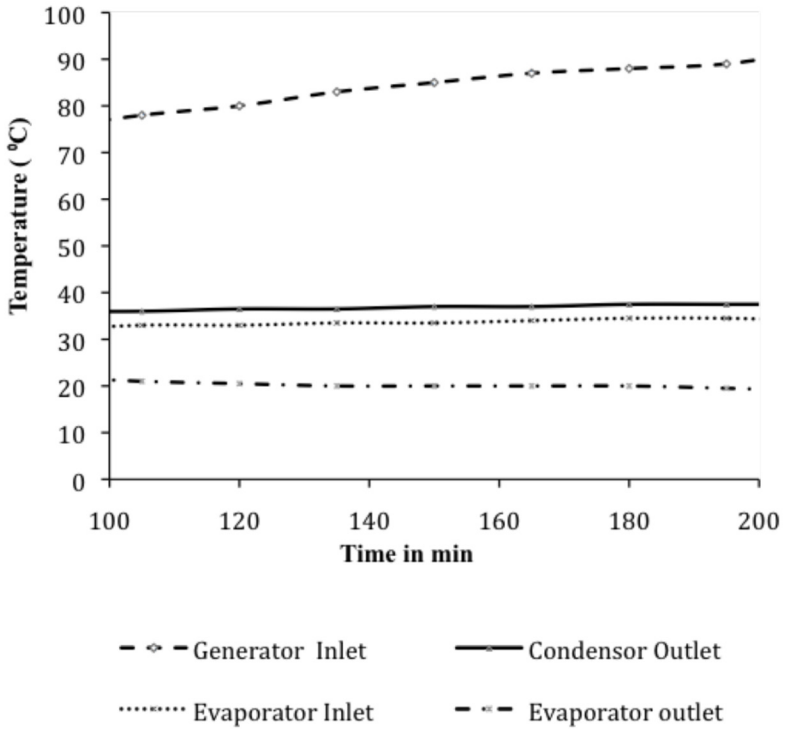


Figure 3. Variation of temperatures of different components against time

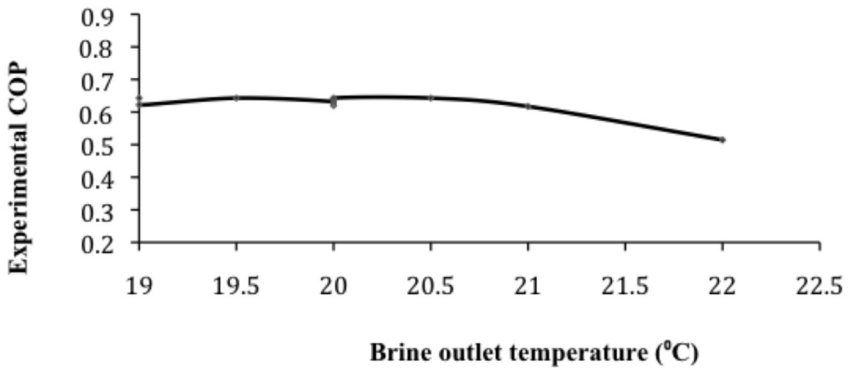


Figure 4. Variation of the experimental COP against brine outlet temperature

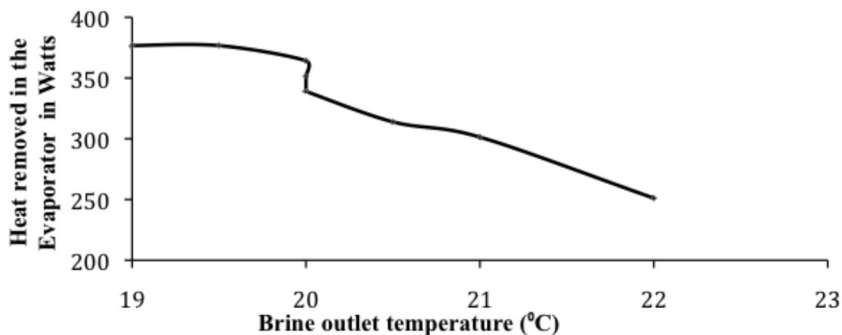


Figure 5. Variation of the heat removed in the evaporator against brine outlet temperature

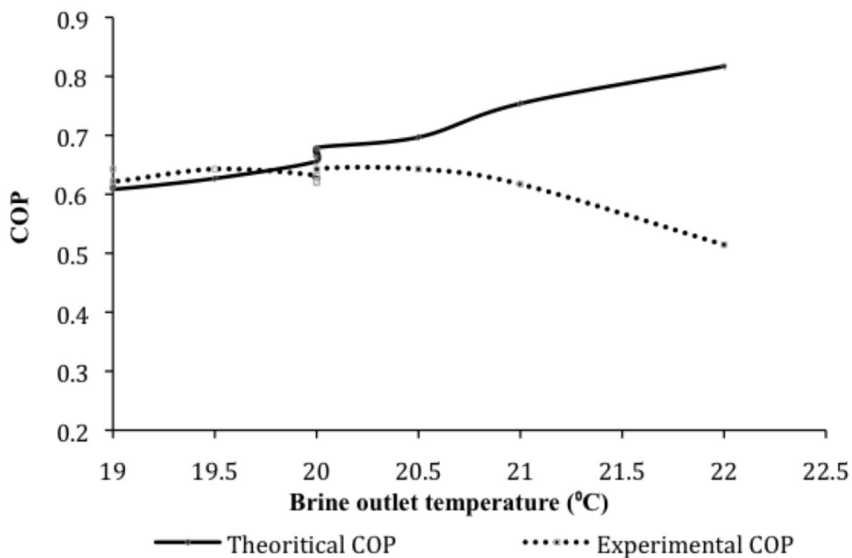


Figure 6. Experimental and theoretical COP against brine outlet temperature

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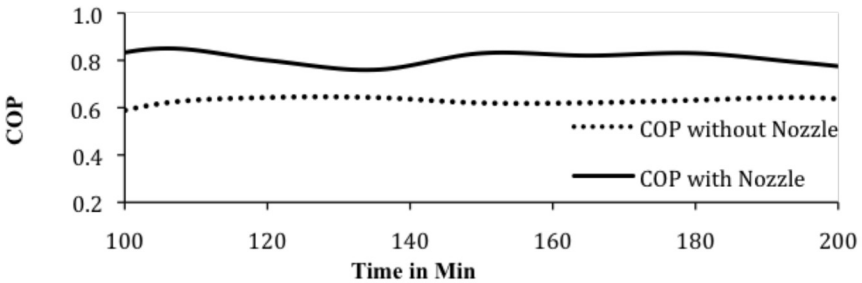


Figure 7. Effect of COP in CSRS With and Without Nozzle

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