
Hypersingular Boundary Integral Equation for Harmonic Acoustic Problems in 2.5D Domains with Moving Sources

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Abstract

A challenge faced when modeling coincident boundaries by the Boundary Element Method, is to obtain an accurate approximation of integrals which have singular and/or hypersingular kernels. In this paper, we apply a procedure based on regularization of the kernels to compute singular and hypersingular integrals for time harmonic wave problems in two and a half dimensional (2.5D) domains. For this purpose, the Fundamental Solution is described and the study of the terms that arise taking its limit as $r \rightarrow 0$ is carried out. These terms lead to Singular Boundary Integral Equation (SBIE) and Hypersingular Boundary Integral Equation (HBIE). Regular terms of SBIE and HBIE are integrated by applying numerical quadratures, whereas singular and hypersingular terms are calculated analytically. Working in 2.5D domains make it easier to compute moving sources. A procedure, which leads to a simple change of the frequency of the problem, is described in this paper. Numerical results are presented for acoustic problems with coincident boundaries to demonstrate the accuracy of the proposed formulation.

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1 Introduction

There is no doubt that noise pollution is a serious problem in our society. There are many diseases related to the increment of noise near housings [1]. Acoustic barriers are built to reduce or eliminate rail or car traffic noise. Thus, a good tool to estimate it is needed, in order to improve life quality in the cities. Many authors have studied the modeling of acoustic barriers; Finite Differences Method and Finite Element Method (FEM) were often used on this purpose. When Boundary Element Method [2, 3] appeared, new ways to address the problem were developed. A great advantage of this method when compared to FEM is that an infinite domain can be modeled easily, satisfying the far-field conditions, without having to increase the number of elements. This is why BEM is used in this paper to model sound propagation in air.

Acoustic barriers, which pursue the aim of restricting noise levels, are often modeled as an infinitely thin domain [4]. In BEM formulation, this would lead to a pair of infinitely close boundaries which are called *Coincident Boundaries*. Although BEM shows strong performance in wave propagation analysis problems, modeling these special boundaries using BEM leads to the integration of functions with hypersingular kernels, which are not easy to compute. For this purpose, many authors have proposed different techniques to face this problem. Gray [5] uses a linear function to represent the integrand function over the domain; [6] presents a regularization of the kernels by using simple solutions; [7] use polar transformation and Lauren expansion series are used to derive the hypersingular integral; [8] employ image source technique to avoid hypersingular terms. In this work, we apply the regularization procedure presented by [9] for the purpose of computing singular and hypersingular integrals in two and a half dimensional (2.5D) domains.

Another important issue when facing traffic noise calculations is estimating the effect of a moving emitting source. As traffic is composed by different moving sources such as cars or buses, it is needed to study the impact of their speed on the modeling problem. Some authors propose different ways to study this issue. Andersen and Nielsen [10] study the ground noise produced by a train load using moving coordinates. Tadeu et al. [11] use a 3D incident field in order to calculate sound absorption when the source is moving at constant speed in 2.5D problems. An interesting result is suggested by [12], who use source loads activated in different time-steps to simulate a moving load. In

this paper, we propose a procedure to convert the moving-source problem into a fixed source problem which could be used in 2.5D domains problems. Although this work shows the formulation for the particular case of acoustic barriers, this procedure can also be applied to any wave propagation problem in 2.5D with coincident boundaries (such as antiplane shear problems near cracks) by just changing the meaning of the variables and constants, provided that the problem follows Helmholtz equation.

2 Boundary Element Formulation

The scalar Helmholtz equation can be written as:

$$\frac{1}{c^2} \frac{\partial^2 p}{\partial t^2} - \nabla^2 p - \frac{1}{c^2} b = 0 \quad (1)$$

In the particular case of 3D acoustics, c is the wave propagation speed inside the fluid, b are the external forces, p is the fluid pressure and $\nabla = \left(\frac{\partial}{\partial x}, \frac{\partial}{\partial y}, \frac{\partial}{\partial z} \right)$. For time harmonic problems, a Fourier Transform along time-axis can be done to convert the problem from time-domain to frequency-domain. Also, if the geometry of the acoustic domain does not vary along z -coordinate, a parameter k_z called wave number can be defined, and making another Fourier Transform along z -axis would lead to:

$$P(x, y, k_z, \omega) = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} p(x, y, z, t) e^{-i(\omega t - k_z z)} dz dt \quad (2)$$

This formulation express the solution of (1) as an infinite sum of waves with different k_z and ω . Substitution of (2) into (1), assuming there is no external forces ($b = 0$) and with some rearrangement, gives the homogeneous Helmholtz equation in 2.5D:

$$\nabla^2 P + k_f P = 0 \quad (3)$$

where $\nabla = \left(\frac{\partial}{\partial x}, \frac{\partial}{\partial y} \right)$ and $k_f = \frac{\omega^2}{c^2} - k_z^2$. Let Γ be the 2D boundary of the acoustic domain, $\mathbf{X} = \{x_i\}$ be a point over Γ , and let $\mathbf{Y} = \{y_i\}$ be the collocation point of the fundamental solution of (3); standard boundary integral equation (PBIES) of this equation is:

$$c(\mathbf{Y})P(\mathbf{Y}) + \int_{\Gamma} Q^*(\mathbf{X}; \mathbf{Y})P(\mathbf{X})d\Gamma(\mathbf{X}) - \int_{\Gamma} P^*(\mathbf{X}; \mathbf{Y})Q(\mathbf{X})d\Gamma(\mathbf{X}) = 0 \quad (4)$$

where $Q = \frac{\partial P}{\partial n}$ is the pressure gradient and $c(\mathbf{Y})$ is the so called “free term”. P^* and Q^* are, respectively, the fundamental solutions for the pressure and the pressure gradient:

$$P^*(\mathbf{X}; \mathbf{Y}) = P^*(r) = \frac{1}{4i} H_0^{(2)}(k_f r)$$

$$Q^*(\mathbf{X}; \mathbf{Y}) = Q^*(r) = \frac{ik_f}{4} \frac{\partial r}{\partial \mathbf{n}} H_1^{(2)}(k_f r)$$

where $H_0^{(2)}$ and $H_1^{(2)}$ are Hankel functions of second kind and r , the Euclidean distance between the point over the domain \mathbf{X} and the collocation point \mathbf{Y} :

$$\mathbf{r} = \mathbf{X} - \mathbf{Y}$$

$$r = |\mathbf{X} - \mathbf{Y}|$$

When there is a rigid barrier inside the domain, its boundary can be expressed as a sum of three parts: the exterior boundary Γ_C and two coincident boundaries (Γ^+ and Γ^-), one for each face of the barrier [13]. As shown in Figure 1, both Γ^+ and Γ^- are infinitely close, so if \mathbf{Y} is over one of these boundaries, (4) leads to an incompatible system of equations. Let $\mathbf{n}^+ = \{n_i\}$ be the normal vector of Γ^+ , then, $-\mathbf{n}^+$ would be the normal vector of boundary Γ^- . Thus, with some rearrangement, (4) when \mathbf{Y} is over the barrier is:

$$\begin{aligned} c(\mathbf{Y})P(\mathbf{Y}) + \int_{\Gamma_C} Q^*(\mathbf{X}; \mathbf{Y})P(\mathbf{X})d\Gamma(\mathbf{X}) + \int_{\Gamma^+} Q^*(\mathbf{X}; \mathbf{Y})P(\mathbf{X})d\Gamma(\mathbf{X}) \\ + \int_{\Gamma^-} Q^*(\mathbf{X}; \mathbf{Y})P(\mathbf{X})d\Gamma(\mathbf{X}) - \int_{\Gamma_C} P^*(\mathbf{X}; \mathbf{Y})Q(\mathbf{X})d\Gamma(\mathbf{X}) \\ - \int_{\Gamma^+} P^*(\mathbf{X}; \mathbf{Y})Q(\mathbf{X})d\Gamma(\mathbf{X}) - \int_{\Gamma^-} P^*(\mathbf{X}; \mathbf{Y})Q(\mathbf{X})d\Gamma(\mathbf{X}) = 0 \end{aligned} \quad (5)$$

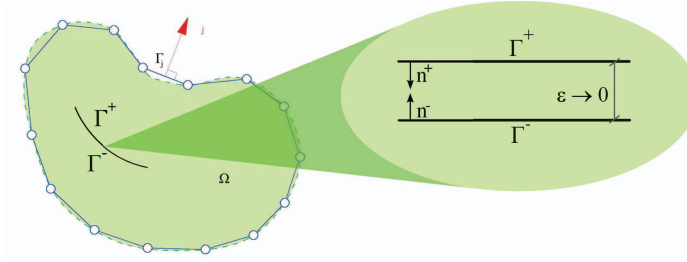


Figure 1 Example of a domain with a barrier on it inside. Both faces of the barrier are infinitely close to each other ($\epsilon \rightarrow 0$).

Calling $\Delta P = P^+ - P^-$ and $\Delta Q = Q^+ - Q^-$, gives (5) as:

$$\begin{aligned} c(\mathbf{Y})P(\mathbf{Y}) + \int_{\Gamma_C} Q^*(\mathbf{X}; \mathbf{Y})P(\mathbf{X})d\Gamma(\mathbf{X}) + \int_{\Gamma^+} Q^*(\mathbf{X}; \mathbf{Y})\Delta P(\mathbf{X})d\Gamma(\mathbf{X}) \\ - \int_{\Gamma_C} P^*(\mathbf{X}; \mathbf{Y})Q(\mathbf{X})d\Gamma(\mathbf{X}) - \int_{\Gamma^+} P^*(\mathbf{X}; \mathbf{Y})\Delta Q(\mathbf{X})d\Gamma(\mathbf{X}) = 0 \end{aligned} \quad (6)$$

Using (6), instead of two separate equations for each face of the barrier, make the system of equation indeterminate. Thus, in order to have a determinate system, a new equation is needed. For this purpose, (6) can be derived with respect to \mathbf{Y} over the direction defined by the vector $\mathbf{N} = \{N_i\}$, which is the normal vector in the collocation point. This leads to:

$$\begin{aligned} Q^+(\mathbf{Y}) + \int_{\Gamma_C} \mathcal{S}(\mathbf{X}; \mathbf{Y})P(\mathbf{X})d\Gamma(\mathbf{X}) + \int_{\Gamma^+} \mathcal{S}(\mathbf{X}; \mathbf{Y})\Delta P(\mathbf{X})d\Gamma(\mathbf{X}) \\ - \int_{\Gamma_C} \mathcal{D}(\mathbf{X}; \mathbf{Y})Q(\mathbf{X})d\Gamma(\mathbf{X}) - \int_{\Gamma^+} \mathcal{D}(\mathbf{X}; \mathbf{Y})\Delta Q(\mathbf{X})d\Gamma(\mathbf{X}) = 0 \end{aligned} \quad (7)$$

where

$$\mathcal{S}(\mathbf{X}; \mathbf{Y}) = \frac{\partial}{\partial y_i} Q^*(\mathbf{X}; \mathbf{Y}) N_i \quad (8a)$$

$$\mathcal{D}(\mathbf{X}; \mathbf{Y}) = \frac{\partial}{\partial y_i} P^*(\mathbf{X}; \mathbf{Y}) N_i \quad (8b)$$

and the summation convention for repeated indices is adopted. Equation (6) is called Gradient Boundary Integral Equation (QBIES). The main disadvantage of using QBIES formulation is that it yields integrals with hypersingular kernels. A way to avoid this obstacle is proceed as follows. First, (8a) has to be expressed as a combination of Hankel functions:

$$\mathcal{S}(\mathbf{X}; \mathbf{Y}) = \frac{-ik_f}{4} \left[\frac{1}{r} \left(n_i - 2 \frac{\partial r}{\partial \mathbf{n}} r_{,i} \right) H_1^{(2)}(k_f r) + \frac{\partial r}{\partial \mathbf{n}} k_{f,i} H_0^{(2)}(k_f r) \right] N_i \quad (9)$$

where $r_{,i} = \frac{\partial r}{\partial x_i}$. In order to get non-regular terms of (9), Lauren expansion of its Hankel functions has been done. Two non-regular terms have been obtained:

- $\frac{1}{2\pi r^2} n_i N_i$ which is **hypersingular**
- $\frac{-k_f^2}{4\pi} n_i N_i \log(r)$ which is **singular**

Both terms are regularized and integrated following the procedure described in [9]. The same procedure has to be done with (8b). Expressing it as a combination of Hankel functions:

$$\mathcal{D}(\mathbf{X}; \mathbf{Y}) = \frac{ik_f}{4} H_1^{(2)}(k_f r) r_i N_i \quad (10)$$

In this case, after making a Lauren expansion of this function, all resultant terms are regular. Thus, no special integration is needed and integrals can be calculated numerically.

3 Numerical Examples

In order to show the accuracy of the previous method, we have calculated a theoretical example. Let us consider a 2.5D domain where there is a rigid barrier. Assuming ω , k_z and c given boundary conditions expressed in Figure 2, and all units according to the International System of Units; we are going to compare results obtained after an analysis with both PBIES and QBIES. In the case of PBIES, the barrier can be modeled as an elliptical boundary where its semi-minor axis $b \rightarrow 0$. On the other hand, for a QBIES formulation, the barrier will be modeled as a pair of coincident boundaries, as shown previously.

After both analysis, we show the results for the base boundary ($y = 0$), and for the barrier in Figure 3. Also, we have calculated the pressure in some internal points (Figure 4).

As we can see in Figures (3–4), as long as the semi-minor axis b tends to 0, PBIES results tend to the solution with QBIES formulation. When b is too small, the system of equations obtained with PBIES formulation is

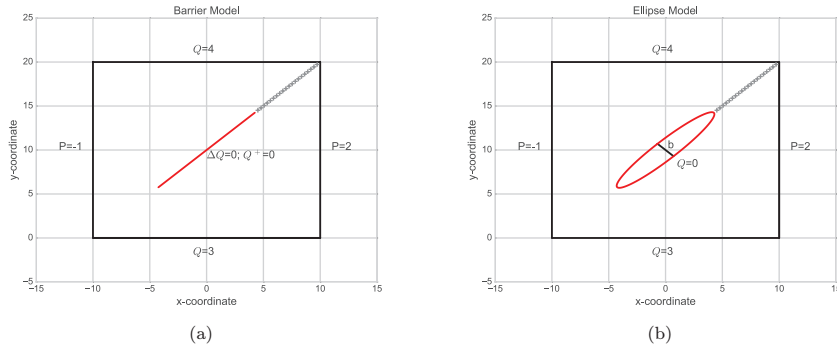


Figure 2 (a) Model with a pair of coincident boundaries and its boundary conditions. (b) Model with elliptical barrier. Crosses are internal points, where P will be calculate.

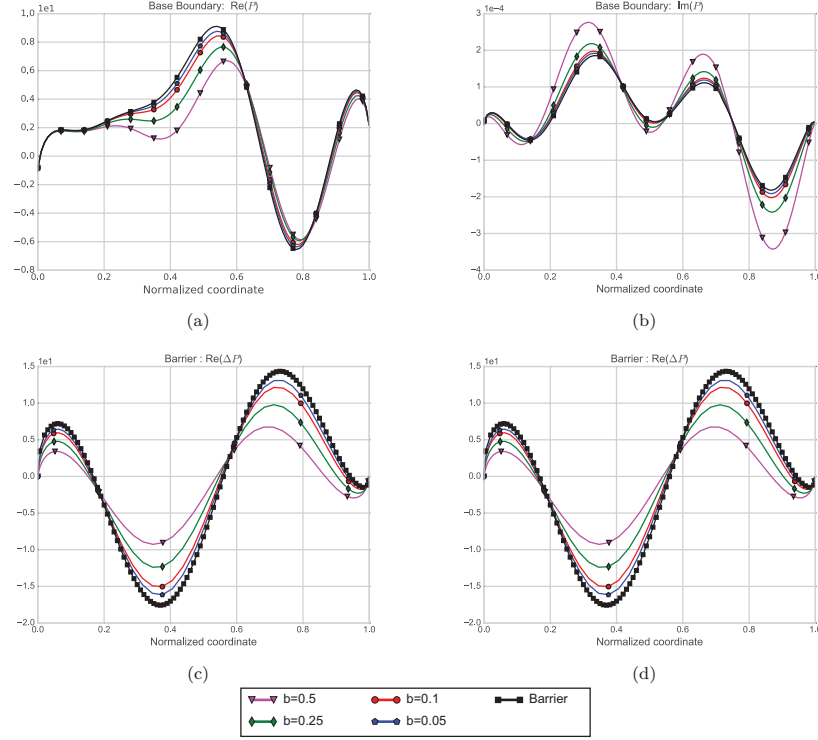


Figure 3 Comparison between P calculated with QBIES, and PBIES for different b values. (a) and (b) show real part and imaginary part respectively, of P in base boundary. (c) and (d) show real part and imaginary part respectively, of ΔP in the barrier. Dimension of both boundaries have been normalized from 0 to 1.

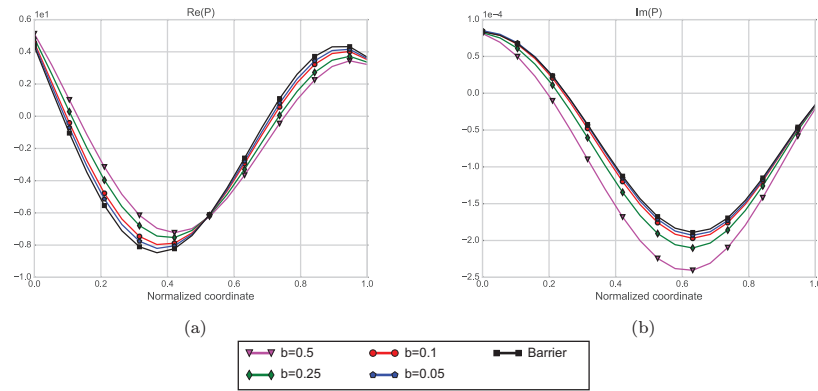


Figure 4 Comparison between P obtained in internal points calculated with QBIES, and PBIES for different b values. Distance from the barrier has been normalized from 0 on the left and down to 1 on the right and up. (a) shows the real part and (b) shows the imaginary part.

not consistent. In contrast, coincident boundaries formulation has a better performance, as the barrier is already infinitely thin. Thus, the accuracy of the results is better.

4 Moving Sources

One of the main advantages of working in 2.5D domains is when applied loads are moving constantly along one coordinate. Traffic noise problems can belong to these kind of situations. Let us have a 3D acoustic domain with an invariant geometry along z direction, and a point load moving with v constant speed along z direction. If we call $p_m(x, y, z - vt, t)$ and $P_m(x, y, k_z, \omega)$ the applied moving load in 3D domain and in 2.5D domain, respectively; and we follow the procedure described in Section 2 to work in ω and k_z domain:

$$P_m(x, y, k_z, \omega) = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} p_m(x, y, z - vt, t) e^{-i(\omega t - k_z z)} dz dt \quad (11)$$

making the appropriate change of variables $z' = z - vt$ in previous equation:

$$\begin{aligned} P_m(x, y, k_z, \omega) &= \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} p_m(x, y, z', t) e^{-i(\omega t - k_z(z' + vt))} dz' dt \\ &= \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} p_m(x, y, z', t) e^{-i(\overbrace{(\omega - k_z v)}^{\Omega} t - k_z z')} dz' dt = P(x, y, k_z, \Omega) \end{aligned} \quad (12)$$

where $P(x, y, k_z, \Omega)$ is the solution for a fixed load (Section 2) with Ω frequency. Thus, being $k_f'^2 = \frac{(\omega - k_z v)^2}{c^2} - k_z^2$, Helmholtz differential equation results:

$$\nabla^2 P + k_f' P = 0$$

As a consequence of the previous demonstration, the moving source problem, when working in 2.5D domains, can be solved using the fixed source formulation (Section 2) by just changing ω for $\Omega = \omega - k_z v$. In order to illustrate how to proceed when a moving source is applied to a 3D domain, the following example is given. Let us have a street where an acoustic barrier separates a building from a highway as shown in Figure 5(a). Let us consider a

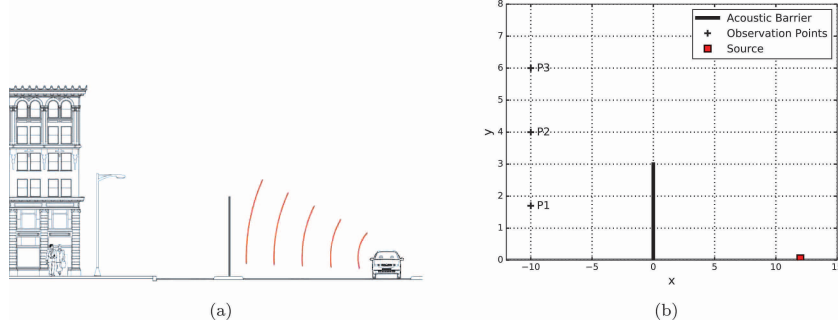


Figure 5 (a) Example problem. (b) Diagram of the problem in a 2.5D dimension model, crosses are observation points where the solution will be computed.

given source of frequency f moving at constant speed v and three observation points represented in Figure 5(b). Let also consider there is no air flux through the ground and the barrier, thus boundary conditions in both boundaries would be $Q = 0$. Using the formulation described in precedent sections, we are going to calculate the noise reduction resulting from the insertion of an acoustic barrier between the highway and the building for several values of v : 140, 120, 100, 80, 60 [km/h]. Insertion loss (IL) [4] is determined as follows:

$$IL = -10 \log_{10} \left(\frac{\langle p_f^2 \rangle}{\langle p_0^2 \rangle} \right) [\text{dB}] \quad (13)$$

where $\langle p_0^2 \rangle$ is the mean squared pressure without the barrier and $\langle p_f^2 \rangle$ is the mean squared pressure with the barrier. A general solution of the problem could be computed by just varying k_z and v . Figure 6(a) represents this solution at the first observation point (height = 1.7 m) when the frequency $\omega = 650$ Hz. For any given v_i , the resultant IL would be the general solution calculated over the equation line $\Omega = \omega - v_i k_z$, as showed in Figure 6(b). Thus, following this procedure, we can obtain the solution at any given frequency ω for any value of v by just evaluating IL over its equation line.

Figures 7–9 show the resultant IL when the solution is evaluated at the three observation points at a frequency ω of 650 Hz. As can be seen, for the same frequency of the source, different values of the speed lead to different solutions of the problem.

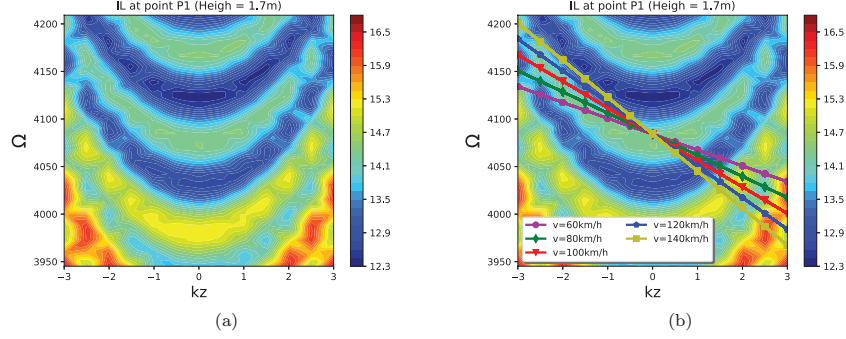


Figure 6 (a) General solution of the problem ($\Delta \Omega = 10$ rad/s and $\Delta k_z = 0.05$ rad/m). Abscissa axis represent k_z , ordinate axis is Ω and color scale is the insertion loss. Image (b) shows different lines, one for each value of v , where IL is evaluated.

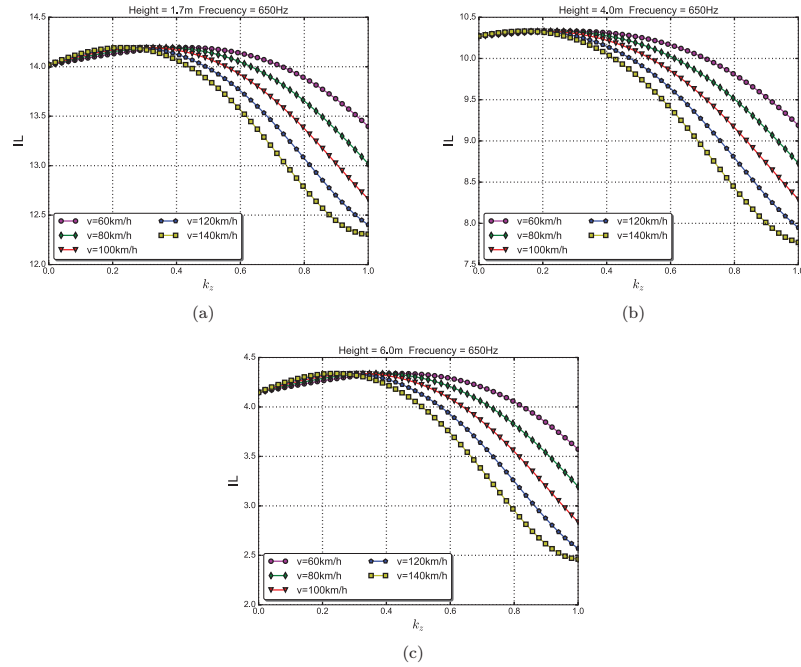


Figure 7 IL evaluated at observation points when the frequency of the source is 650 Hz.

As a final result, an Inverse Fourier Transform of IL along k_z dimension is represented when the speed is 100 [km/h] and the frequency is 450 Hz (Figure 10). We have compute the solution for 256 points varying k_z from -6 to 6 rad/m.

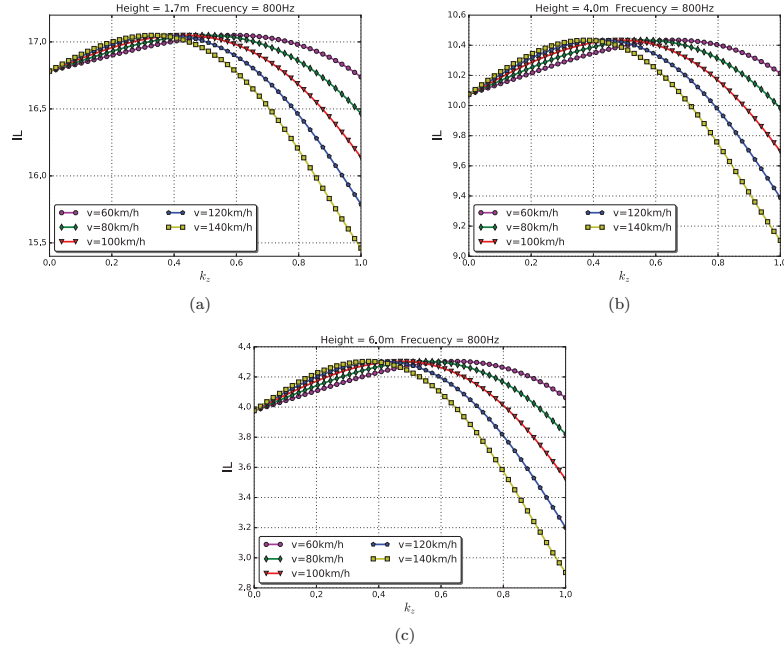


Figure 8 IL evaluated at observation points when the frequency of the source is 800 Hz.

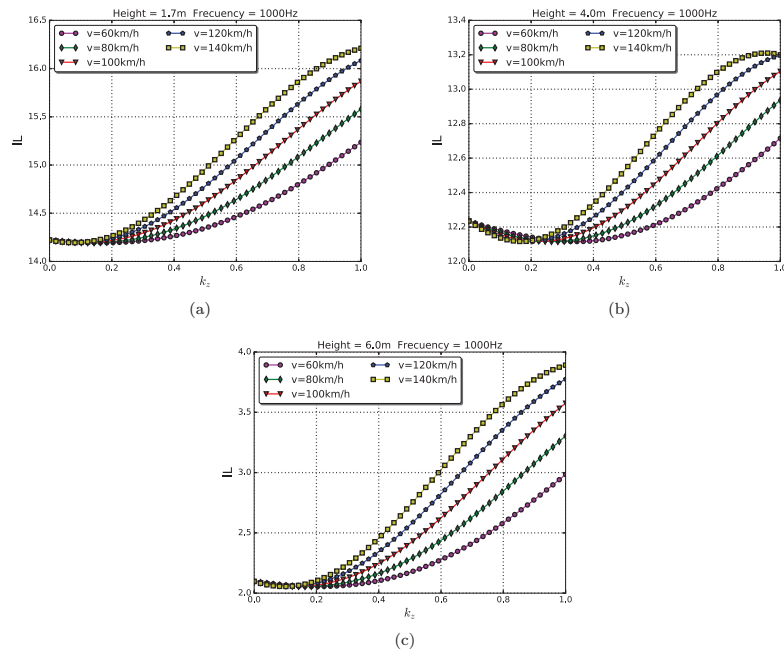


Figure 9 IL evaluated at observation points when the frequency of the source is 1000 Hz.

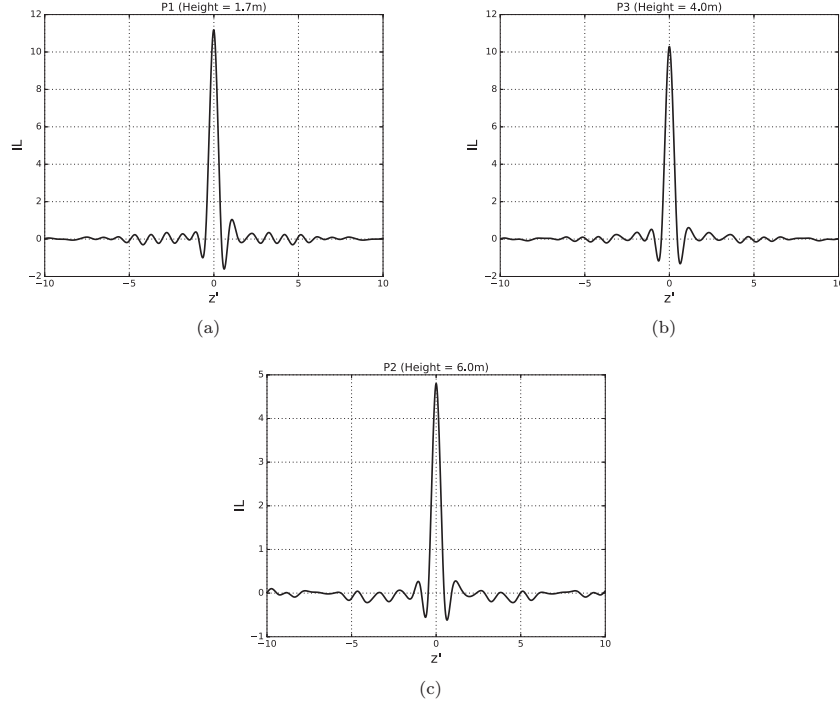


Figure 10 Results in three observation points (P1, P2, P3) on a 3D geometry domain and frequency domain.

5 Conclusions

In this paper, we propose a way to apply the Boundary Element Method to acoustic problems where a barrier is placed to reduce traffic noise. Acoustic barriers are modeled as a pair of infinitely close boundaries that produce integrals whose kernels are hypersingular. The suggested way to solve this kind of integrals is by making a regularization of their kernels, which makes it possible to compute them by numerical integration.

Traffic sound sources, such as cars or trains, can be modeled as point loads moving along one direction parallel to the barrier. Transforming the problem dimension from 3D to 2.5D has the great advantage of allowing the use of a fixed source formulation with a simple modification of the frequency. An example problem has been solved in order to present the method, whose results can be seen in Figures 7–9. These figures show the effect of the speed on insertion loss of the acoustic barrier.

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Biographies



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Esther Puertas García is permanent lecturer at the University of Granada. She received her Bachelor and Master degrees in Civil Engineering at the University of Granada, and PhD degrees in Civil Engineering from the University of Granada in 2014. She has an extensive teaching, research and professional experience in the Mechanics of Continuous Media and Theory of Structures topics. Her research work concerns the development of computational toolkits for continuum media dynamics. She belongs to the Research Group of Mechanics of Solids and Structures. Her lines of work are based on the study of Integral Equations Methods for advanced applications in Solid Mechanics. She has developed techniques for the analysis of wave propagation problems in two and a half domains.



Rafael Gallego is full professor at the University of Granada since 1995. He received his Bachelor and Master degrees in Structural and Mechanical Engineering at the University of Sevilla (1987) and got his PhD at the same University in 1990; he was granted a Fulbright postdoctoral scholarship (1990–92) at the Brown University. Among other academic posts, he has been chairman of the Department of Structural and Hydraulic Engineering at the University of Granada since 2000 to 2008 and since 2016 to date. His research work has focused in developing computational models based on Boundary Integral Equations for solid mechanics problem, mainly related to wave propagation in solids, dynamic fracture mechanics and dynamic soil-structure interaction, including resolution of inverse problems to match computational results and experimental ones.

