
Optimal Placement of Distributed Generators and Capacitors for Power Loss Reduction Using Crested Porcupine Algorithm

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Abstract

In recent years, as the need for energy rises, the application of dispersed generation and shunt capacitors has become a more common solution to meet the growing demand of energy. The article presents a novel approach to optimise radial distribution networks, called the Crested Porcupine optimisation algorithm (CPOA), inspired by the behaviour of the Crested Porcupine. The proposed method is tested on the IEEE system, which has 33, 69 and 85 buses. The purpose of this work is to lower the cost and power loss while improving the voltage profile and voltage stability index (VSI) using the Capacitor Banks (CB) and Distributed Generator (DG) units at the correct location and of appropriate size. Inclusion of load models is also taken into consideration.

Keywords: Voltage profile, power loss, distributed generation, capacitor bank and voltage stability index.

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Nomenclature and Abbreviations

CPOA	Crested porcupine optimization algorithm	IA	Improved Analytical
VSI	Voltage stability index	SSO	Shark Smell Optimization
CB	Capacitor bank	AT	Analytical Technique
DG	Distributed generation	I_n	Branch current
RDN	Radial distribution network	R_n	Branch resistance
MO	Multi objective	N_b	Number of buses
MFO-SCA	Moth flame optimization and Sine Cosine algorithm	RPL	Reduction in power loss
ECOA	Enhanced Coyote optimization algorithm	TVD_{base}	Total base voltage deviation
GA	Genetic algorithm	RPL_{base}	Total base reduction in power loss
PSO	Particle swarm optimization	P_{DG}^{min}	Minimum active power from DG
IMDE	Intersect mutation differential evolution	P_{DG}^{max}	Maximum active power from DG
RPL	Reduction in power loss	Q_{DG}^{min}	Minimum reactive power from DG
VSI	Voltage stability index	Q_{DG}^{max}	Maximum reactive power from DG
TVD	Total Voltage deviation		

1 Introduction

On a global scale, insufficiency of power is a well-known issue. This problem is because of the enormous demand for electrical energy. This high demand cannot be met by a centralised power supply. To overcome this issue, distribution networks play an important role. It results in lower voltages and high-power loss. Generally, distribution networks are connected with many kinds of loads, such as commercial, residential, and industrial. The above-mentioned loads are dependent on voltage. After changing the load profile on the demand side, voltage collapse occurs, resulting in an imbalance of power and voltage profile. To suffice all up to a certain extent, integration of dispersed generation or distributed generation into the distribution network is quite popular [1]. By properly incorporating the DG units into the distribution system, overall efficacy can be improved. Likewise, the radial distribution network can be made more efficient by locating CBs and DGs simultaneously using a multi-objective optimization strategy [2].

Many previous literatures are discussed here in brief. Whale optimization and polar bear optimization are described in [3] and [4], respectively, for different bus systems to allocate the capacitors. Using the 24-bus system and the spotted hyena optimizer algorithm, different loading situations are also taken into account in [5]. To achieve the minimum real power loss, an analytical expression and exact loss calculation are given in [6] for the individual allocation of dispersed generators in RDN. for minimization of losses and improvement in voltage profile on IEEE 33,69 and 118 bus systems, simulated annealing and comprehensive teaching-learning based optimization algorithms, respectively, are suggested in [7] and [8]. For the purpose of assigning appropriate sized DG on the 86 bus and 69 bus system, [9] demonstrates multi-objective (MO) optimization employing adaptive particle swarm optimization and a modified gravitational search technique. [10] integrates DG and CBs at the same time to reduce power loss in IEEE 69 and 33 bus distribution systems by implementing a hybrid technique called MFO-SCA (Moth flame optimisation algorithm and sine cosine algorithm). In [11] ECOA is implemented on different distribution systems containing 33, 69, and 85 buses for solving the MO problem. Objectives are to reduce loss and cost and to improve the stability of voltage. [12] and [13] both allocate DG and CB simultaneously using soft-computing techniques such as GA, PSO and cuckoo search optimization, respectively, to find the target. [22] presents an African vultures optimization technique to optimally allocate DG and capacitor banks on 85 and 118 bus systems for minimizing total system cost, and active and reactive line loss. [23] introduces a novel optimization method known as IMDE designed to optimally position and size DGs and CB inside the distribution network. [29] described the modified firefly algorithm on the 85-bus system to improve efficiency and voltage profile. [30] presents Cheetah optimisation on 33 and 69 bus standard distribution systems to achieve the objectives of better power loss and voltage stability.

In the presented approach, the CPOA is implemented to optimize the size and location of type-I DG, type-III DG, CBs, and simultaneous placement of the type-I DG along with CB in different radial networks of distribution system.

2 Problem Formulation

2.1 Power Flow

Radial distribution system has some unique features such as high value of resistance to reactance ratio, unbalanced load, and radial layout.

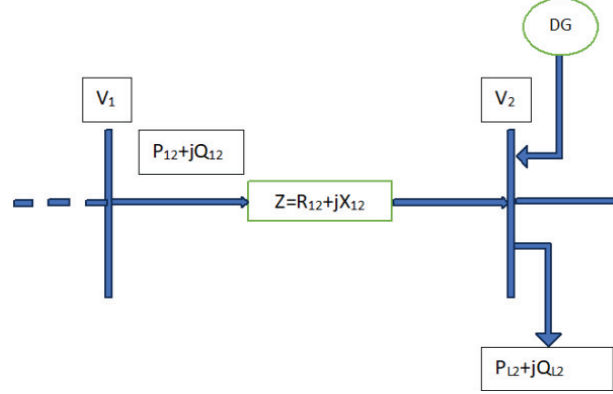


Figure 1 Radial distribution system.

The Forward – backward sweep approach is employed due to the slow convergence of the traditional load flow method. To assess the power from the receiving to the sending end is called forward sweep, while reverse assessment of voltage is under forward sweep.

Figure 1 shows radial distribution system with two buses namely bus 1 and bus 2. Active and reactive power flow between bus 1 and 2 denoted by P_{12} and Q_{12} via branch and bus voltage, can be calculated using Equations (1) to (2), as below

$$P_{12} = P_2 + P_{L2} + R_{12} \left[\frac{(P_2 + P_{L2})^2 + (Q_2 + Q_{L2})^2}{|V_2|^2} \right] \quad (1)$$

$$Q_{12} = Q_2 + Q_{L2} + X_{12} \left[\frac{(P_2 + P_{L2})^2 + (Q_2 + Q_{L2})^2}{|V_2|^2} \right] \quad (2)$$

Here,

P_2 and Q_2 are real and reactive power of bus 1 and bus 2.

V_1 and V_2 are voltage of bus numbers 1 and 2, respectively

P_{L2} and Q_{L2} are real and reactive power of load connected in second bus

R_{12} and X_{12} are the resistance and reactance of the branch connected between bus 1 and 2

$$P_{12} = P_2 + P_{L2} + R_{12} \left[\frac{(P_2 + P_{L2})^2 + (Q_2 + Q_{L2})^2}{|V_2|^2} \right] - P_{DG2} \quad (3)$$

Real power with installation of type 1 DG only, type 3 DG only, type 1 and CB simultaneously, can be shown as Equation (3)

$$Q_{12} = Q_2 + Q_{L2} + X_{12} \left[\frac{(P_2 + P_{L2})^2 + (Q_2 + Q_{L2})^2}{|V_2|^2} \right] - Q_{cap_2} \quad (4)$$

Equation (4) shows reactive power flow after inserting only the capacitor bank and the simultaneous insertion of type 1 and capacitors.

After the DG installation of type 3

$$Q_{12} = Q_2 + Q_{L2} + X_{12} \left[\frac{(P_2 + P_{L2})^2 + (Q_2 + Q_{L2})^2}{|V_2|^2} \right] - Q_{DG_2} \quad (5)$$

Reactive power flow can be found by Equation (5) when only type 3 DG is inserted.

Here, P_{DG_2} and Q_{DG_2} represents real and reactive power injection from DG, and Q_{cap_2} denotes reactive power injection from CB.

Proper installation of DG can effectively support the system performance improvement, such as voltage profile, stability, and power quality [33].

2.2 Objective Function

Now, the objective function can be defined as Equation (6) given below,

$$F = f1 + f2 + f3 + f4 \quad (6)$$

here,

$$f1 = \frac{RPL}{RPL_{Base}}, \quad f2 = \frac{TVD}{TVD_{Base}},$$

$$f3 = \frac{VSI^{-1}}{VSI_{Base}^{-1}} \quad \text{and} \quad f4 = aP_{DG}^2 + bP_{DG} + c;$$

and the values of $a = 0$, $b = 20$ & are $c = 0.25$.

Where,

$$RPL = \sum_{n=1}^{Nb} I_n^2 R_n$$

$$TVD = \sum (V_{ref} - Final \text{ voltage})$$

$$VSI = V_1^4 - 4(P_2 X_{12} - Q_{12} R_{12})^2 - 4(P_2 R_{12} - Q_2 X_{12})|V_1|^2$$

Here, RPL is the reduction in power loss, and VSI is the voltage stability index. TVD is the total voltage deviation, equivalent to the summation of the difference between V_{ref} and the final voltage of all the buses.

2.3 Constraints

There are several limitations related to the goal that can be grouped into two types: Equality and inequality constraints, shown in Table 1.

Table 1 Constraints under the study

Constraints	Name	Relation
Equality	Power balance	$P_{TL} + \sum P_D(n) = \sum P_{DG/Cap}(n)$ & $Q_{TL} + \sum Q_D(n) = \sum Q_{DG/Cap}(n)$
Inequality	Bus voltage & Thermal limit	$V_{min} \leq V_i \leq V_{max}$ and $I_i \leq I_{max\ i}$
	DG capacity limit	$P_{DG}^{min} \leq P_{DG} \leq P_{DG}^{max}$ & $Q_{DG}^{min} \leq Q_{DG} \leq Q_{DG}^{max}$
	Capacitor bank capacity	$Q_{capacitor}^{min} \leq Q_{capacitor} \leq Q_{capacitor}^{max}$

3 Crested Porcupine Optimization (CPO)

Crested porcupine optimization (CPO) is an innovative meta-heuristic technique to solve the optimization problem involving large-scale data sets, evolved by Mohamed Abdel-basset et al. [27]. Crested porcupines shown in Figure 2 are the third largest rodent, following the capybara and the beaver. CPs are giant, slow, and spherical in shape. The majority of CPs have bristles that are either black or dark brown and occasionally appear with white marks. Their most distinctive feature is the broad quills, which may grow up to 14 inches long and run along the back half of their body. The primary characteristic of CPO is the defense strategy of other animals, such as tigers, leopards, and lions. CPs are the most effective defenders. They are regarded as accomplished defenders due to their unique physical traits. As CPs feel threatened, it adapt their defensive tactics through four displays that show aggression.

It is based on numerous protective actions of the CP, namely sight, sound, odour, and physical attack, ranging from minimal hostile to highly aggressive. The first two methods (i.e. sight and sound) show exploring behaviour, whereas the third and fourth ones (i.e. odour and physical attack) are considered exploitative.



Figure 2 Crested porcupine.

- (i) Vision: It is the very first line of defense. After detecting danger, it defends itself by raising sharp and pointed spines and by elevating its quills to look bigger than they actually.
- (ii) Voice: CPs use a wide range of vocalization tactics to notify predators of their impending arrival. On feeling frightened or hostile, CP creates sounds of whining, grunting, coughing, and snoring, and these become louder. They click their teeth, jump erratically, stamp their feet, and make a loud hissing sound with tail quills to survive and protect themselves.
- (iii) Smell: When visual and audio stimuli don't work to repel a predator, this tactic is used. A foul chemical odour is released by CP's lower back gland. This strategy is often a successful one for fending off dangers.
- (iv) Attack: The distinct characteristic of CP is having powerful quill armour, by using these sturdy quills, CP protects itself against potential danger. When approached by a predator, the CP forms a crest and erects its quills to look larger.

CPO has some benefits such as being less sensitive to parameters, consistent, good balance between exploration and exploitation and global search ability. Also, it has some disadvantages like faces problems while dealing with high dimension problem, and it has fast convergence with untuned parameters. Point-wise elaboration of the benefits of CPOA over the standard metaheuristics given below:

- (i) Maintain balance between exploration and exploitation: CPOA has two local exploitation operators along with two global exploration operators. This makes CPOA superior to the other algorithms (such as GSA, PSO and SSA) suffers from local optima trapping.
- (ii) Enhanced local optima trapping: Due to the incorporation of a cyclic population reduction strategy, some individuals are removed and re-enter for maintenance of the diversity of the population. Due to this

mechanism, CPOA does not face the problem of local minima, unlike other algorithms (PSO, GSA).

- (iii) Less sensitive to parameters: It shows robust performance in different parameter settings. Due to this, CPOA shows lower risk for poor performance in case of improper selection of parameters, unlike other algorithms.
- (iv) Higher speed and convergence: CPOA can achieve a solution very close to the true global optimum in a short time span, and it can achieve a lower mean fitness value and standard deviation than other algorithms (PSO, GSA and SSA)

CPOA has some phases, represented by Equations (7) to (13) described below:

3.1 Initialization

The very first step is the establishment of a population of candidate solutions within the search space. It can be generated at random or using prior information about the issue space.

$$\vec{X}_i = \vec{L} + \vec{r}(\vec{U} - \vec{L}); \quad i = 1, 2 \dots N \quad (7)$$

where,

$\vec{X}_i$ – candidate solution of the search space

L & U – The maximum and lower limits of the search space

$\vec{r}$ – Random vector (within the limit 0 & 1)

3.2 Cyclic Population Reduction Technique

This phase involves the reintroduction of some CPs which are removed from the population to speed up convergence and to avoid the situation of local minima.

$$N = N_{min} + (N - N_{min}) \left(1 - \left(\frac{t \bmod \frac{T_{max}}{T}}{\frac{T_{max}}{T}} \right) \right) \quad (8)$$

N & N_{min} – Size of population and its minimum value.

T & t – Total number of cycles and current function value, respectively.

T_{max} & mod – Function evaluation max. value and the modulo operator, respectively.

3.3 Exploration

This step reveals the exploratory method of the CPO. If the predator is far away, then the CPO can use its eyes or ears to ward off its attacker. It allows searching for promising regions that may involve the near-optimal solution.

- (i) First shield: To find unexplored locations, this option promotes exploring remote regions that may involve desired solutions. This nature is modelled mathematically as follows:

$$\overrightarrow{X_i^{(t+1)}} = \overrightarrow{X_i^{(t)}} + \tau_1 \times |(2 * \tau_2 * \overrightarrow{X_{CP}^{(t)}} - \overrightarrow{y_i^{(t)}})| \quad (9)$$

$\overrightarrow{X_i^{(t+1)}}$ – Location of the i th individual during the $(t + 1)$ th iteration

$\overrightarrow{X_i^{(t)}}$ – Location of i th individual during t th iteration

$\overrightarrow{X_{CP}^{(t)}}$ – Appropriate result for function evaluation t

$\overrightarrow{y_i^{(t)}}$ – A vector to denote the location of a predator during t th iteration

- (ii) Second shield:

$$\overrightarrow{X_i^{(t+1)}} = (1 - \overrightarrow{U_1}) * (\overrightarrow{X_i^{(t)}} \overrightarrow{U_1}) * (\overrightarrow{y} + \tau_3 * (\overrightarrow{X_{r1}^{(t)}} - \overrightarrow{X_{r2}^{(t)}})) \quad (10)$$

$\overrightarrow{U_1}$ – Binary-valued vector.

3.4 Exploitation

In this step, two defence mechanisms, namely odour and physical attack, are considered.

- (i) Third shield:

$$\begin{aligned} \overrightarrow{X_i^{(t+1)}} &= (1 - \overrightarrow{U_1}) * \overrightarrow{X_i^{(t)}} + \overrightarrow{U_1} \\ &\quad * (\overrightarrow{X_{r1}^{(t)}} + S_i^{(t)} * (\overrightarrow{X_{r2}^{(t)}} - \overrightarrow{X_{r3}^{(t)}}) - \tau_3 * \overrightarrow{\delta} * \gamma_t * S_i^{(t)}) \end{aligned} \quad (11)$$

$$\gamma_t = 2 \times rand \times \left(1 - \frac{t}{t_{max}}\right)^{\frac{t}{t_{max}}} \quad (12)$$

$r1, r2, r3$: Randomly generated value between 1 and N

δ – Controlling parameters for searching direction

γ_t & $S_i^{(t)}$ – Defending factor and odour diffusion factor

(ii) Fourth shield:

$$\overrightarrow{X_i^{(t+1)}} = \overrightarrow{X_{CP}^t} + (\alpha(1 - \tau_4) + \tau_4) * (\delta * \overrightarrow{X_{CP}^{(t)}} - \overrightarrow{X_i^{(t)}}) - \tau_5 * \delta * \gamma_t * \overrightarrow{F_i^{(t)}} \quad (13)$$

 α – Convergence speed factor

For ease, the location updating process of porcupine can be understood by Equation (14)

$$\overrightarrow{x_i^{t+1}} = \begin{cases} \begin{cases} \overrightarrow{\text{Apply Equation (9)}} \\ \overrightarrow{\text{Apply Equation (10)}}, & \tau_6 < \tau_7 \quad \tau_8 < \tau_9 \text{ (Exploration)} \\ \text{Else} \end{cases} \\ \overrightarrow{\begin{cases} \text{Apply Equation (11)} \\ \text{Apply Equation (13)}, & \tau_{10} < T_f \quad \tau_9 \leq \tau_8 \text{ (Exploitation)} \\ \text{Else} \end{cases}} \end{cases} \quad (14)$$

$\tau_1, \tau_2, \tau_3, \tau_4, \tau_5, \tau_6, \tau_7, \tau_8, \tau_9, \tau_{10}$ are the randomly distributed number varying between 0 and 1.

Pseudocode of CPOA

Start

Set the parameters like $N, T_f, T_{\max}, N_{\min}, \alpha, T$;

Randomly initializing the position of the solution $X^i, i = 1, 2, \dots, N$;

While ($t < T_{\max}$)

Find fitness value for candidate solutions.

Find the best solution ($\overrightarrow{x_{cp}^t}$);

Modify Υ_t using Equation (12)

Modify the size of the population with Equation (8)

For $i = 1; N$ do

Update the $m, S, F, \vec{\delta}$;

Generate τ_8 and τ_9 as a random one

If $\tau_8 < \tau_9$ %% Phase: Exploration

Generate τ_6 and τ_7 as a random one

If $\tau_6 < \tau_7$ %% Defensive stage no 1

Apply Equation (9)

Else %% Defensive stage no 2

Apply Equation (10)

Else %% Phase: Exploitation

Create a random number, τ_{10}

```

    If  $\tau_{10} < T_f$  %% Defensive stage no 3
        Apply Equation (11)
    Else %% Defensive stage no 4
        Apply Equation (13)
    End If
    If  $f(\vec{x}_l^{t+1}) > f(\vec{x}_l^t); 1$ 
         $(\vec{x}_l^{t+1}) = (\vec{x}_l^t);$ 
    End if
     $t = t + 1$ 
End for
End while
Return  $(\vec{x}_{cp}^t)$ 
Stop

```

4 Result and Discussion

The proposed Crested Porcupine Optimization Algorithm (CPOA) was implemented and evaluated on IEEE standard test systems, including 33-, 69-, and 85-buses. The single-line diagram along with the data of these bus systems is given in [14]. Taking line and bus data into consideration, a MATLAB code is developed with MATLAB R2021b 64-bit (win 64) and trialled on Intel (R) Core (TM) i3-8100 CPU @ 3.60 GHz with 4.0 GB RAM loaded with Windows 10 Pro. The code has been executed for 30 consecutive trials, and the results are then compiled. The MATLAB code is trialled over seven load model conditions: full load constant power, half load constant power (CPx0.5), overload constant power (CPx1.6), constant current (CC), constant impedance (CI), residential (R), commercial (C), and industrial (I) load.

Here, four cases are considered based on the implementation of compensating units into the system listed below:

- Case 1: Incorporation of type-I DG individually into the system.
- Case 2: Incorporation of type-III DG into the system.
- Case 3: Implementation of only CB into the system.
- Case 4: Simultaneous incorporation of type-I DG along with CB into the system.

Simulation studies for these cases, carried out over the three mentioned systems, are given below. Tables 2, 4, and 6 give the comparative study for test systems I, II, and III.

4.1 Test System I: 33 Bus Standard Radial Distribution Network

The IEEE 33 bus system consists of 32 branches having active and reactive power of 3.72 MW and 2.3 MVar, respectively. Fig. 3 shows a power flow diagram of this system. The line and bus statistics are taken from Baran and Wu [15]. The value of power loss is 202.67 MW for the base case, when any compensation is not connected to the system.

4.1.1 System with type-I DG incorporation (case 1)

The real power loss obtained by the proposed technique is 71.61 kW which shows 64.66% reduction from the base case. The proposed method gives better results than other literatures, shown in Table 2. Total voltage deviation (TVD) and voltage stability index obtained are 0.4391 and 0.9163, respectively.

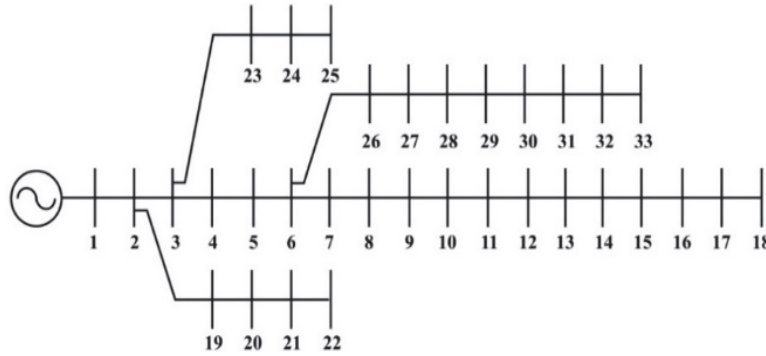


Figure 3 Single-line diagram of the IEEE 33 bus radial distribution system.

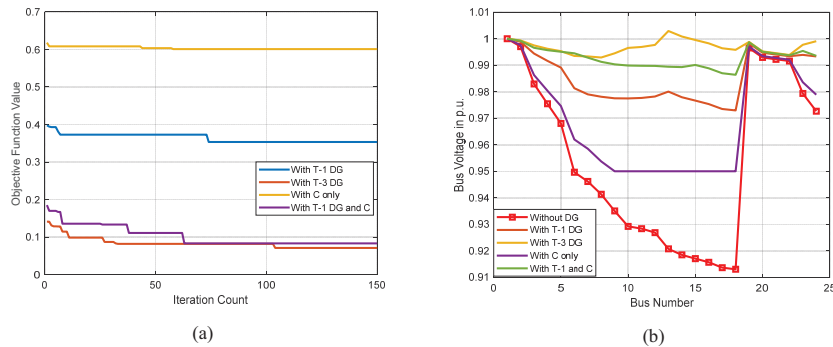


Figure 4 Objective Function characteristics and Bus Voltage Profile for 33 bus system.

Table 2 Comparative study of CPOA for the 33-bus system at full load constant power

Case	Parameters	CPO Proposed	[25] CTLBO	[19] WIPSO GSA	[15] MFO-SCA	[31] KH
1	Size MW	0.82(13)	0.80(13)	0.84(13)	1.05(30)	0.81(13)
	(Site)	1.06(24)	1.09(24)	0.86(24)	1.09(24)	0.84(25)
		1.08(30)	1.05(30)	0.86(30)	0.80(13)	0.84(30)
	PL	71.61	72.79	74.78	72.78	75.41
	%RL	64.66	64.08	64.56	65.5	64.25
	V _{min}	0.969 (33)	–	–	0.9687(33)	0.961(33)
	TVD	0.5677	–	–	–	–
	VSI	0.8819	0.8805	–	–	–
	Cost(\$/MWh)	59.682	59.05	51.45	59.05	50.05
2		CPO Proposed	[34] IA	[13] WIPSO GSA	[32] LSFSA	[31] KH
	Size	0.74/0.55(13)	1.09(6) pf-0.82 lag	1.02(12) pf-0.85 lead	1.19/0.69(6)	0.85/0.49(13)
	MW/MVAR	0.87/0.65(24)	1.09(30) pf-0.82 lag	1.03(24) pf-0.84 lead	0.47/0.27(18)	0.90/0.51(24)
	(Site)	1.07/0.80(30)	0.76(14) pf-0.82 lag	1.08(30) pf-0.8 lead	0.92/0.53(30)	0.89/0.51(30)
	PL	14.38	22.29	16.48	26.7	19.57
	%RL	92.90	89.45	92.19	87.34	90.72
	V _{min}	0.9929 (8)	–	–	0.982(25)	0.9816(33)
	TVD	0.1204	–	–	–	–
	VSI	0.9719	–	–	–	–
3		CPO Proposed	[18] EGWO-PSO	[19] WIPSO GSA	[15] MFO-SCA	[39] WCA
	Size	0.44(57)	0.42(13)	0.47(12)	1.00(30)	0.40(14)
	MVAR	0.66(62)	0.56(24)	0.53(29)	0.33(24)	0.45(24)
	(Site)	0.33(18)	1.14(30)	0.53(30)	0.38(13)	1.0 (30)
	PL	121.83	132.17	141.84	138.91	130.91
	%RL	39.88	34.79	32.78	34.16	35.40
	V _{min}	0.95(9)	0.9377(18)	–	0.9307(18)	0.951(18)
	TVD	1.1529	–	–	1.2711	–
	VSI	0.8145	0.775	–	–	–
4		CPO Proposed		[24] AT	[28] GA	[39] WCA
	Size	0.57(15)/0.78(30)	NA	0.12(12)	DG 0.25(16),	0.56(11)/0.53(14)
	MW(Site)/	1.27(29)/0.25(10)		0.24(12)	0.25(22), 0.5(30)	0.97(25)/0.46(23)
	MVAR(Site)	0.83(25)/0.57(26)			SC 0.3(15),	1.04(29)/0.56(30)
					0.3(18), 0.3(29),	
					0.6(30), 0.3(31)	
	PL	16.83		71.93	71.25	24.69
	%RL	91.69		63.8	64.83	87.82
	V _{min}	0.9864 (18)		0.9815(8)	0.971	0.980(33)
	TVD	0.2092		–	–	–
	VSI	0.9467		–	–	–
	Cost(\$/MWh)	53.77		7.45	20.25	51.65

4.1.2 System with type-III DG incorporation (case 2)

Highest loss reduction of 92.90% is achieved by using the proposed method, which shows better results than previous research paper outcomes. The minimum value of voltage is 0.9929 at bus number 8. Cost is 54.23 \$/MWh, which is lower than other compared papers except [15], while [15] gives a high value of active power loss compared to the proposed one.

4.1.3 Incorporation of only the capacitor bank (CB) into the system (case 3)

Power loss and cost for this case using the proposed algorithm are 121.83 kW and 28.85 \$/MWh, which is far better than other compared literature. It shows better performance of CPOA. Minimum voltage of value 0.95 is obtained at the 9th bus of the system.

4.1.4 Simultaneous integration of type-I with capacitor bank (case 4)

Though the cost of DG is on the higher side in this case for the proposed method, the loss value is much lower than the others, which is equal to 16.83 KW. It also shows the highest percentage of reduction in loss from the base value. At bus number 18, the value of $V_{\min}$ is 0.986 p.u.

In the load model consideration, it can be seen that lower values for power losses are obtained when type 3 DG is inserted into the distribution system. But percentage loss reduction is highest in the constant current case, where the loss is reduced from the base case value by 92.53%.

4.2 Test System II-69 Bus Test System

The next test system used is a radial distribution system having 69 nodes with a base voltage of 12.66 kV and a base kVA of 100 MVA, as depicted in Figure 5. For the 69-node RDS, standard line and bus data are referred from Baran and Wu et al. [39]. This system has real and reactive power loads of 3802.19 kW and 2694.6 kVAr. Real and reactive power losses for the base case are 225 kW and 102.16 kVAr, respectively. The minimum value of voltage at bus 65 is 0.909 for the base case.

4.2.1 System with type-I DG incorporation (case 1)

The real power loss obtained by the proposed technique is 70.77 kW which shows 68.54% reduction from the base case. The proposed method gives better results than other literature, as shown in Table 4. Value obtained for $V_{\min}$ is 1 p.u. at bus number 1. Total voltage deviation (TVD) and voltage stability index obtained are 0.4391 and 0.9163, respectively.

4.2.2 System with type-III DG incorporation (case 2)

Achieved power loss and % loss reduction are 6.87 kW and 96.9434%, which is better than all other research outcomes except [31] and [34]. But the cost

Table 3 Outcomes of the 33-bus system for load models

Cases	Base Case (in kW)	T-1 Only	Unit Size (MW)/[Site]	T-3 only	Unit Size (MW/MVAr)/[Site]	T-1 and C	Unit Size MW[Site]/ MVAr [Site]
CPx0.5 load	47.07	17.070	0.59(29), 0.41(13), 0.42(24)	4.85	0.37/0.23(24), 0.38/0.23(15), 0.47/0.29(30)	6.33	0.25(16)/0.17(32), 0.80(6)/0.24(11), 0.33(32)/0.20(29)
C Px1.6 load	575.367	164.05	1.23(27) 1.40(8) 1.45(24)	54.39	1.42/0.88(25), 1.47/0.91(11), 1.32/0.82(31)	55.78	1.43(13)/1.05(31), 0.87(25)/1.10(4), 1.32(32)/1.08(9)
CC	174.76	62.49	0.61(14) 0.97(30) 0.95(24)	13.22	0.84/0.52(24), 0.63/0.39(14), 1.20/0.74(30)	18.34	0.56(11)/0.14(9), 1.03(29)/0.60(8), 0.76(24)/0.72(30)
CI	151.10	55.03	0.77(30) 0.85(25) 0.87(12)	13.00	0.83/0.51(24), 0.86/0.53(30), 0.87/0.54(11)	15.66	0.80(15)/0.42(6) 0.76(25)/0.65(31) 0.84(30)/0.28(17)
R	154.44	43.47	0.72(13) 1.01(30) 0.86(24)	12.77	0.93/0.58(24), 0.50/0.31(14), 0.97/0.60(30)	16.64	0.84(25)/0.90(3) 0.59(32)/0.62(29) 1.16(10)/0.32(13)
C	157.85	48.49	0.75(29) 0.73(13) 0.92(25)	17.16	0.38/0.23(17) 0.95/0.59(25) 1.12/0.69(29)	21.51	1.01(30)/0.75(30) 1.09(25)/0.38(18) 0.57(8)/0.45(25)
I	148.79	36.30	0.76(14) 0.93(30) 0.90(24)	12.70	0.67/0.32(14) 0.97/0.47(30) 1.31/0.63(24)	16.95	0.76(33)/0.56(23) 0.99(11)/0.40(7) 1.41(24)/0.54(31)

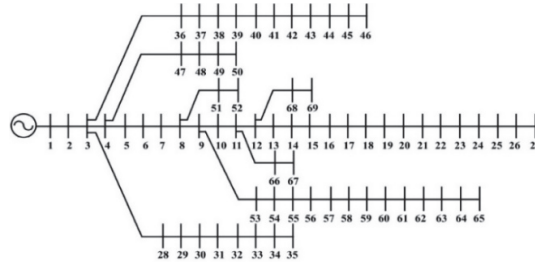


Figure 5 Connection diagram of an IEEE distribution system having 69 buses.

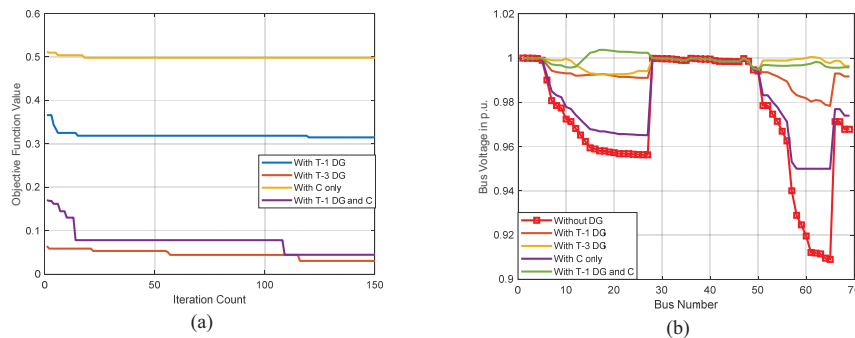


Figure 6 Objective Function characteristics and Bus Voltage Profile for 69 bus

from the proposed one is 52.88 \$/MWh, which is lower than the above-mentioned papers, which shows a better result in economical point of view. The minimum value of voltage is 0.9926 at bus number 18.

4.2.3 Incorporation of only CB into the system (case 3)

Power loss and cost for this case using the proposed algorithm are 111.99 kW and 28.25 \$/MWh, which is far better than other compared literature. It shows better performance of CPOA. Minimum voltage of value 0.95 is obtained at the 58th bus of the system, which is also a better value.

4.2.4 Simultaneous integration of type-I with capacitor bank (case 4)

The percentage reduction in power loss obtained by the proposed algorithm is 95.53%, which shows the best performance of the proposed technique compared to previous literature shown in the table. It also shows the highest percentage of reduction in loss from the base value. Though the cost of DG is on the higher side in this case for the proposed method, the loss value is

Table 4 Comparative study of CPOA for the 69-bus system at full load constant power

Case	Parameters	CPO Proposed	[23] IMDE	[1] JAYA-IWO	[32] LSFSA	[33] ECOA
1	Size	0.45(18)	1.73(61)	0.47(23)	0.42(18)	0.74(14)
	MW	0.44(11)	0.473(20)	0.34(69)	1.33(60)	0.65(25)
	(Site)	1.70(62)		1.71(61)	0.42(65)	1.07(30)
	PL	70.77	70.92	70.92	77.1	71.8
	%RL	68.54	68.47	68.47	65.72	68.08
	V _{min}	1.0(1)	0.9808(65)	0.979(65)	0.9811(61)	0.9784
	TVD	0.4391	—	—	—	—
	VSI	0.9163	—	—	—	—
	Cost(\$/MWh)	52.29	44.31	50.65	43.65	49.45
2		CPO Proposed	[34] IA	[18] EGWO-PSO	[32] LSFSA	[31] KH
	Size	0.69/0.42(10)	2.07(61) pf-0.82 lag	0.77(13)	0.54(18)	0.56(11)
	MW/MVAR	1.74/1.08(61)	0.62(17) pf-0.82 lag	1.07(24)	1.19(60)	0.35(22)
	(Site)	0.19/0.12(25)	0.82(50) pf-0.82 lag	1.03(30)	0.31(65)	1.77(61)
	PL	6.87	4.95	11.68	16.26	5.92
	%RL	96.9434	97.74	94.24	92.76	92.8
	V _{min}	0.9926(18)	—	0.9926(8)	0.9885(61)	0.9943(50)
	TVD	0.1542	—	—	—	—
	VSI	0.9707	—	0.9707	—	0.9772
	Cost(\$/MWh)	52.88	70.45	57.65	41.05	53.85
3		CPO Proposed	[23] IMDE	[18] EGWO-PSO	[35] PVSC, DGPI	[21] WCA
	Size	0.44(57)	1.26(61)	0.42(11)	0.35(50)	1.28(61)
	MVAR	0.66(62)	0.37(21)	0.25(20)	1.05(61)	0.21(69)
	(Site)	0.33(18)		1.41(61)	0.39(64)	0.27(18)
	PL	111.99	145.53	145.13	66.74	144.53
	%RL	50.21	35.2	35.5	33	28.68
	V _{min}	0.95(58)	0.9330(65)	0.9314(65)	0.97	0.95(65)
	TVD	1.3282	—	—	—	0.698
	VSI	0.8145	—	0.7841	—	0.961
	Cost(\$/MWh)	28.25	32.85	41.85	36.05	35.45
4		CPO Proposed	[23] IMDE	[36] Fuzzy GA	[35] PVSC, DGPI	[21] WCA
	Size	0.69(17)/0.17(21)	1.73(62)/0.10(63)	1.58/1.13	1.85/1.79	0.54(17)/1.18(2)
	MW(Site)/	0.20(50)/1.10(61)	0.47(24)/1.19(61)			2(61)/1.23(62)
	MVAR(Site)	1.70(62)/0.06(69)				1.15(69)/0.26(69)
	PL	10.05	13.83	19.18	9.63	33.33
	%RL	95.53	93.84	91.47	91	85.18
	V _{min}	0.9948(50)	0.9915(68)	0.9859(65)	0.99	0.994(50)
	TVD	0.0759	—	—	—	0.0071
	VSI	0.9795	—	0.9846	—	0.965
	Cost(\$/MWh)	52.39	44.25	31.94	37.25	74.25

much lower than the others, which is equal to 10.05 kW except [35]. At bus number 50, the value of V_{min} is 0.9948 p.u.

4.3 Test System III: 85-Bus Radial Distribution Network

In Figure 8, the single-line diagram of the 85-bus network is given. For the line and bus data, [16] is referred to as an 85-bus standard test system having 85 nodes and 84 branches. 12.66 kV and 100 MVA, respectively, are the

Table 5 Outcomes of the 69 bus RDS with load models

Load Model	Base Case (in kW)	Cases					Unit Size MW[Site]/ MVar [Site]	
		T-1 Only	Unit Size (MW)/[Site]	T-3 only	Unit Size (MW/MVar)/[Site]	T-1 and C		
CPx0.5 load	51.59	18.22	0.80(61)	2.74	0.41/0.31(12)	6.71	0.75(64)/0.82(3)	
			0.46(3)		0.87/0.65(61)		0.27(38)/0.74(63)	
			0.46(13)		0.23/0.17(46)		0.38(13)/0.46(29)	
C Px1.6 load	652.41	172.85	0.79(17)	36.57	0.82/0.61(14)	70.52	0.58(21)/1.00(63)	
			0.91(55)		1.19/0.89(61)		1.03(64)/0.07(54)	
			1.19(56)		1.01/0.75(62)		1.12(62)/0.90(12)	
CC	188.60	63.30	1.08(62)	8.16	1.18/0.89(61)	13.7	0.55(14)/1.10(51)	
			0.56(13)		0.35/0.26(16)		0.95(64)/0.34(19)	
			0.51(64)		0.32/0.24(63)		0.75(61)/0.83(61)	
CI	158.74	52.81	0.40(64)	7.50	0.32/0.24(57)	12.62	0.98(60)/1.13(61)	
			1.08(61)		0.48/0.36(16)		0.57(12)/1.61(11)	
			0.41(21)		1.16/0.87(62)		0.56(64)/0.96(34)	
R	164.82	43.84	0.91(63)	12.18	0.52/0.39(20)	13.05	1.11(61)/0.93(61)	
			0.97(12)		1.14/0.85(61)		0.32(68)/0.12(5)	
			0.68(58)		0.85/0.63(49)		0.48(18)/0.57(12)	
C	156.88	43.80	0.49(64)	7.28	0.33/0.25(21)	12.31	0.61(58)/0.69(61)	
			0.91(61)		1.19/0.89(61)		0.84(62)/0.16(17)	
			0.58(16)		0.63/0.47(66)		0.55(15)/0.55(60)	
I	173.3384	44.52	0.89(33)	15.37	1.08/0.81(9)	15.91	0.59(31)/0.17(14)	
			0.49(72)		0.32/0.24(73)		0.52(79)/0.39(33)	
			0.61(11)		0.60/0.45(35)		0.61(26)/0.47(63)	

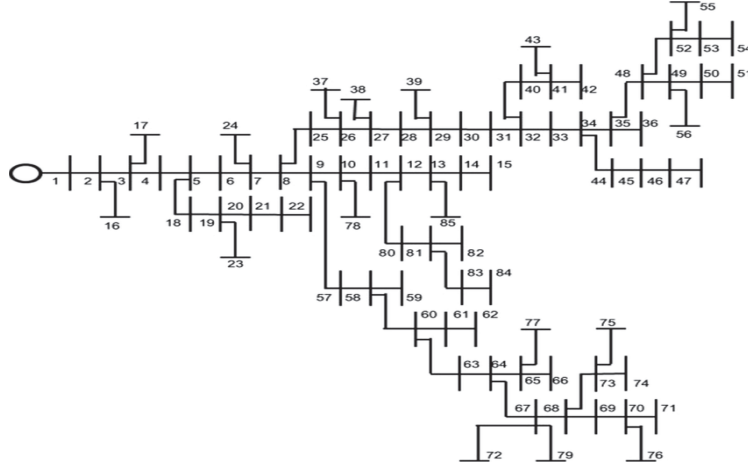


Figure 7 Single-line diagram of radial network having 85 buses.

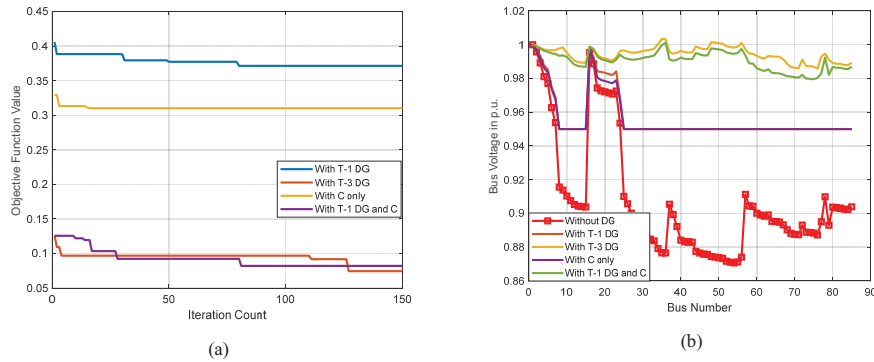


Figure 8 Objective Function characteristics and Bus Voltage Profile for 85 bus.

values of base voltage and base kVA in this system. This system has active and reactive power of the loads are 2.5703 MW and 2.6222 MVAR. In the base case, active and reactive power losses are 316 kW and 198.57 kVAR, respectively.

4.3.1 System with type-I DG incorporation (case 1)

The real power loss obtained by the proposed technique is 117.43 kW which shows 62.85% reduction from the base case. The proposed method gives the best result in terms of power loss reduction than other literature. Value of obtained cost is 34.93 \$/MWh, which also shows better result than other

Table 6 Comparative study of CPOA for the 85-bus system at full load constant power

Case	Parameters	CPO	[37] AQIEA	[17] WOA	[19] WIPSO GSA	[20] MFF
1	Size	1.10(7)	0.68(66)	0.94(55)	0.59(26)	1.0(9)
	MW/	0.36(3)	0.95(25)		0.60(34)	0.70(33)
	(Site)	0.26(23)	0.64(34)		0.59(67)	0.50(61)
	PL	117.43	151.89	224.04	152.38	151.79
	%RL	62.85	51.95	–	51.07	51.86
	V _{min}	0.95 (8)	–	0.9109	–	0.9435
	TVD	3.68	–	–	–	–
	VSI	0.81	–	–	–	0.7923
	Cost(\$/MWh)	34.93	45.65	19.05	35.85	44.25
2	Size	0.76/0.57(35)	NA	1.289(55)	0.89(26)	NA
	MW/MVAR	1.18/0.89(9)			0.85(35)	
	(Site)	0.4/0.3(64)			0.89(64)	
	PL	23.98		157.485	20.19	
	%RL	92.54		50.11	93.52	
	V _{min}	0.9858 (78)		0.9255	–	
	TVD	0.4698		–	–	
	VSI	0.9446		–	–	
	Cost(\$/MWh)	47.39		26.03	52.85	
3			[38] PSO	[17] WOA	[19] WIPSO GSA	[20] MFF
	Size	0.83(7)	1.04(9)	DGII-	0.60(25)	1.00(9)
	MVAR	0.36(35)	0.67(34)	0.87(55)	0.60(35)	0.70(33)
	(Site)	0.40(60)	0.56(64)		0.60(67)	0.45(61)
	PL	98.05	151.19	229.02	153.79	154.06
	%RL	68.98	52.17	27.45	50.62	51.15
	V _{min}	0.95 (8)	–	0.903	–	0.9171
	TVD	3.72	–	–	–	–
	VSI	0.81	–	–	–	0.7074
	Cost(\$/MWh)	32.05	45.65	17.65	36.25	43.25
4			[40] GABC		[19] WIPSO GSA	[29] SSO
	Size	0.47(10)/0.73(9)	0.57(36)/0.3(53)	NA	0.50(27)/0.43(29)	0.95(9)/0.94(9)
	MW(Site)/	0.69(36)/0.77(36)	1.20(56)/0.45(46)		0.50(35)/0.45(36)	0.7(33)/0.72(33)
	MVAR(Site)	0.80(57)/0.51(69)	0.42(54)/0.3(54)		0.50(67)/0.51(67)	0.47(61)/0.50(61)
	PL	25.99	73.24		37.27	20.98
	%RL	91.77	76.85		88.21	93.35
	V _{min}	0.9795 (75)	0.9612		0.964	0.9855
	TVD	0.812	2.3139		–	–
	VSI	0.920	0.8546		–	0.9431
	Cost(\$/MWh)	39.76	44.05		30.25	42.65

papers except [17]. But power loss is very high in [17]. So the proposed method shows better performance.

4.3.2 System with type-III DG incorporation (case 2)

Highest loss reduction, i.e. 92.54% is achieved by using the proposed method, which shows better results than previous research paper outcomes. The minimum value of voltage is 0.858 at bus number 78. Cost is 47.39 \$/MWh,

Table 7 Results of 85 bus RDN with Load Model

Load Model	Base Case (in kW)	Cases					Unit Size MW[Site]/ MVar [Site]
		T-1 Only	Unit Size (MW)/[Site]	T-3 only	Unit Size (MW/MVar)/[Site]	T-1 and C	
CP x0.5 load	66.54	34.50	1.07[68,9,49]	5.79	1.23/0.94 [67, 32, 9]	8.17	1.0 [48, 26, 8]/ 0.99 [80, 59, 42]
C Px1.6 load	932.25	243.47	2 [7,58,6]	69.33	3.25/2.44 [34,67,82]	75.25	2.67[49,26,65]/ 3.12[68,49,59]
Constant Current	233.32	107.99	1.15 [20,60,7]	20.71	1.94/1.45 [34,26,64]	28.05	2.42[67,32,46]/ 1.72[72,7,33]
Constant Impedance	182.74	92.00	1.65 [65,9,31]	17.77	1.72/1.29 [32,8,67]	20.56	1.68[34,8,55]/ 1.71[77,57,36]
Residential	175.13	62.03	1.96 [72,8,35]	11.53	1.7/1.27 [67,12,32]	17.69	1.67[32,31,60] / 1.44[70,9,32]
Commercial	168.53	69.66	1.66[64,9,36]	12.23	1.81/1.36 [11,64,31]	17.44	1.81[55,63,9]/ 1.24[67,59,49]
Industrial	173.84	47.50	1.89[49,12,72]	14.48	1.9/1.42 [32,64,9]	15.91	1.72[31,79,2]/ 1.03[14,33,63]

which is lower than other compared papers except [17], while [17] gives a huge value of active power loss compared to the proposed one.

4.3.3 Incorporation of only the capacitor bank into the system (case 3)

Power loss for this case using the proposed algorithm is 98.05 kW, which is far better than other compared literature. It shows better performance of CPOA. Minimum voltage of value 0.95 is obtained at the 8th bus of the system. Total voltage deviation (TVD) and voltage stability index obtained are 3.72 and 0.81, respectively.

4.3.4 Simultaneous integration of type-I with a capacitor bank (case 4)

Though the cost obtained by the proposed method, i.e. 39.76 \$/MWh is on the higher side than [19], the achieved loss by the proposed algorithm is far better than [19], which is equal to 25.99 kW. At bus number 75, the value of $V_{\min}$ is 0.9795 p. u. Total voltage deviation and VSI obtained are 0.812 and 0.920, respectively.

The various load models are studied for individual DG integration and the optimal simultaneous DG and capacitor placement. Tables 3, 5 and 7 represent the line losses for various load models for bus systems I, II, and III, respectively, except the constant power (full load) model. Figures 3, 6 and 9 represent the objective function for all three-bus system i.e. 33 bus, 69 bus and 86 bus systems. Likewise Figures 4, 7 and 10 represent the voltage profile for all three-bus system i.e. 33 bus, 69 bus and 86 bus systems.

5 Conclusion

In this article, CPOA shows better results in achieving the desired objective function in a successful manner for optimal placement of compensating units. The efficacy of the method is tested on various load models, and the results are verified with the previous research articles. The power losses are minimized effectively, and voltages are also improved over buses. TVD and VSI are also calculated and found effective. The cost for a total number of units is calculated and compared to many previous methods, and it is found to be lesser. Moreover, the proposed methodology presents an electrically and economically viable solution for the optimal placement of DGs, switched capacitors, and the simultaneous operation of the two. The application of the

proposed method and likely algorithms to an unstable system could be the future scope of the work.

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Biography



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